# **Engineering Models for Titan's Atmosphere**

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This report presents engineering models for Titan's atmospheric structure used in the design and analysis of the Huygens Probe and its mission. It supersedes an earlier report by Lellouch & Hunten published in 1987 (hereafter LH; also see the Lellouch & Runten paper in this volume). There has been significant progress in our under-standing of Titan's atmosphere in the last few years, particularly in the thermal structure of the upper atmosphere and in the chemical composition of the atmosphere. We make use of these advances in constructing the new models.

These models will be used in the study of two problems: the Probe's heat loading during atmospheric entry, and the descent time to the surface. The first problem concerns primarily the atmospheric structure below 600 km, and the second the atmospheric structure in the lowest 200 km. If the models are to be used for other purposes, the authors should be consulted.

As in the LH report, we present three models: a recommended model; a model for maximum mass density; and a model for minimum mass density. The minimum and maximum models also have the lowest and highest temperatures. It is an assumption on our part that atmospheres with the minimum and maximum possible mass densities and temperatures will produce extreme values for heat loading and descent times of the Huygens Probe.

The models are based on observations made by the Voyager 1 radio science subsytem (RSS), infrared spectrometer (IRIS) and ultraviolet spectrometer (UVS). The recommended model provides an adequate fit to all three data sets.

#### 2.1 Temperature profile

The thermal structure of Titan's atmosphere below 200 km altitude can be inferred from the RSS occultation measurements. The inference of temperatures in this manner depends upon the atmosphere's composition. The thermal structure of Titan's atmosphere at altitudes from 120 km to 300 km is also constrained by IRIS measurements of the brightness of the  $CH_4$  band centred at 1304 cm~' (Lellouch et al., 1989). The determination of temperature from these measurements depends on the mole fraction of  $CH_4$  in the Stratosphere. The thermal structure at altitudes above 1000 km was measured by the UVS solar occultation experiment (Smith et al., 1982; Strobel et al., 1992). In addition to these direct measurements, the different regions of the atmosphere must be connected by the equation of hydrostatic equilibrium. Finally, we require that the temperature profile bears a resemblance to profiles based on theoretical calculations. We first discuss determination of the thermal structure from the measurements, hydrostatic equilibrium and theoretical calculations for an assumed composition, then discuss UVS and IRIS constraints on the atmospheric composition.

Results from the RSS occultation experiment constitute the primary data set used in determination of the temperature profile at altitudes below 200 km. Analysis of these data has determined the refractivity of

# 1. Introduction

## 2. Recommended Model

the atmosphere (Lindal et al., 1983). The RSS experiment measured the refractivity of the atmosphere during both ingress and egress occultations. Although there are slight differences between the ingress and egress occultation at altitudes above 150 km, they are small compared with other uncertainties in the model atmosphere and can be ignored. Thus we will rely upon the RSS ingress data exclusively for determination of atmospheric structure below 200 km.

We infer number densities from the refractivity data through

$$R(z) = \sum N_i(z)\alpha_i \tag{1}$$

where z is altitude, R(z) is the measured refractivity,  $N_i(z)$  number density of the *i*th constituent, and is the refractivity of the *i*th constituent. We use values for  $\alpha_i$  of 294, 277 and 430 x 10<sup>-6</sup> for  $N_i$ , Ar and CH<sub>4</sub>, respectively.

The pressure is obtained from the mass density through the equation of hydrostatic equilibrium,

$$\frac{dP(z)}{dz} = -\rho(z)g(z),$$
(2)

where P(z) is the pressure,  $\mathbf{r}(z)$  is the mass density, and g(z) is the acceleration of gravity. The temperature, T(z), is obtained from the pressure and number densities through the equation of state,

$$P(z) = N(z)kT(z) / F_c(Z)$$
(3)

where k is Boltzmann's constant and  $N(z) = \sum N_i(z)$  is the total number density. The quantity  $F_c(z)$  is a correction factor that takes account of the non-ideal nature of the gas in Titan's atmosphere. We calculate  $F_c(z)$  in the manner suggested by Lindal et al. (1983).  $F_c(z)$  has a maximum value of about 1.03 at the surface.

At altitudes above 150 km the quality of the RSS data diminishes. This manifests itself primarily as noise in the derived temperature profile. To rectify this problem, we use a smoothed representation of the temperature profile obtained by averaging over the noise in the derived temperature profile. Using this smoothed temperature profile we then solve equation (2) again to obtain pressure and mass density. The values of P(z) and  $\mathbf{r}(z)$  so derived are found to be in excellent agreement with those derived directly from the data.

To model the temperature profile in the upper atmosphere, we take an empirical approach based on the Yelle (1991) physical models for the thermal structure. Yelle (1991) calculated radiativeconductive equilibrium temperature profiles for a variety of conditions and was able to explain successfully several features of the thermal structure. However, these calculations are costly and time-consuming; therefore, we have chosen to model the temperature profile with an empirical function similar to those calculated by Yelle (1991). The empirical temperature profiles are constrained to have a temperature minimum (the mesopause) at 0.3 *m*bar and to be isothermal (i.e. dT/dz = 0) at 1 x 10<sup>-4</sup> *m*bar. The temperature at 7 X 10<sup>2</sup> *m*bar is also treated as a free parameter. Spline interpolation on log pressure is used to calculate temperatures at levels between these three grid points. For all the models considered here the temperature at 1 x 10<sup>-4</sup> *m*bar is set to 175 K (Strobel et al., 1992). The temperature at 0.3 *m*bar is adjusted to fit the IRIS measurements of the CH<sub>4</sub> 1304 cm<sup>-1</sup> band, and the temperature at 0.3 *m*bar is adjusted so that the densities at 1240 km agree with the UVS measurements. The densities at 1240 km depend on the temperature profile at lower altitudes because hydrostatic equilibrium is applied to the entire atmosphere.

#### 2.2 Composition

The UVS occultation measurements determined that Titan's atmosphere is composed primarily of N<sub>2</sub>. There is also evidence for significant quantities of CH<sub>4</sub> from IRIS and UVS data. There is a theoretical expectation that argon is present in the atmosphere, but there has been no direct detection of this atom. However, because it is difficult to detect, argon might still be present in significant amounts (i.e. mole fractions of <10%).

The relative abundance of  $CH_4$  and argon will vary with altitude in the upper atmosphere because of diffusive separation. The relative abundance of  $CH_4$  may also vary with altitude in the troposphere (altitudes below 40 km) because of condensation. Diffusive separation does not become significant until ~600 km; therefore, the mole fraction of argon should be constant at altitudes below 600 km and the mole fraction of  $CH_4$  should be constant in the 40-600 km region.

To model the effects of diffusive separation, we adopt the analytic expression of Strobel et al. (1992; see also Steiner & Bauer, 1990) for the  $CH_4$  and Ar mole fractions as a function of altitude. The  $CH_4$  mole fraction is calculated from

$$f_{CH_4} = A_1 (1 + e^{(1 - \kappa)x})^{\frac{3}{7(1 - \kappa)}} + A_2$$
(4)

and the Ar mole fraction from

$$f_{Ar} = A_3 (1 + e^{(1 - \kappa)x})^{\frac{-0.3}{(1 - \kappa)}}$$
(5)

where  $x = 1.76 \times 10^5 (z - z_h)/((R_T + z_h)(R_T + z))$ , and  $A_1$ ,  $A_2$  and  $A_3$  are integration constants used to match conditions deep in the atmosphere. The parameter  $\kappa$  describes the altitude variation of the eddy diffusion coefficient (Strobel et al., 1992).

The recommended model has a constant  $CH_4$  mole fraction in the troposphere and lower stratosphere. The value of the  $CH_4$  mole fraction is adjusted along with the temperature profile to fit the IRIS spectra. We find that good fits to the IRIS data can be obtained with a mole fraction in the 1-5% range. The UVS data are best fit with a  $CH_4$  mole fraction in the lower stratosphere of 2.6-5.0% (Strobel et al., 1992). Thus, we adopt a  $CH_4$  mole fraction of 3% for the recommended model. A mole fraction of 3% implies some supersaturation in the troposphere; however, the degree of supersaturation is small (a maximum value of 18%) and limited to a 15 km region just below the tropopause. It is possible to remove this difficulty with a more complicated  $CH_4$  distribution but the resulting atmosphere would differ trivially from a model with a constant  $CH_4$  mole fraction; therefore, we have retained this simple model.

Argon is potentially a significant component of Titan's atmosphere. In order that its effects can be evaluated in engineering model studies, we include it in the recommended model with a mole fraction of 2 % in the troposphere and lower stratosphere. However, we emphasise that there is no observational evidence yet for argon in Titan's atmosphere.

#### 2.3 Results

We find that the RSS, UVS and IRIS data can be matched with a model described by the parameters listed in Table 1. The temperature, mass density,  $CH_4$  and argon mole fractions are shown in Figs. 1-3. A fit to the IRIS spectra based on this model is shown in Fig. 4. The surface pressure is 1.46 bar.





Fig. 2. Methane mole fraction profiles with altitude for Titan's atmosphere.



## 3. Maximum and Minimum Models

The uncertainties in our ability to predict the structure of Titan's atmosphere at the time of Huygens' deployment arise from several different causes. First, there are uncertainties in the models caused by uncertainties in the analysis of Voyager data. Second, there may be latitudinal variations in the atmospheric structure not properly accounted for in the models. Third, the atmosphere may exhibit temporal variations. The minimum and maximum models presented here include all three sources of uncertainty.





Fig. 3. Argon mole fraction profiles with altitude for Titan's atmosphere.

Fig. 4. A fit to Voyager's IRIS spectra based on the model described by the parameters given in Table 1.

We construct maximum and minimum models for Titan's atmosphere in several stages. The first step consists of determining the uncertainty in atmospheric densities inherent in the analysis of the RSS occultation experiment. This uncertainty is due almost completely to our lack of knowledge of the relative abundances of the different constituents. Therefore, we first determine the maximum and minimum density profiles consistent with the RSS data and some basic physical constraints on the atmosphere. We join these new models to the upper atmosphere in the same manner as was done for the recommended model. The parameters describing the models are adjusted so that these new models (prior to incorporation of the latitudinal and temporal

variations in temperature) are also consistent with the RSS, IRIS and UVS observations.

To understand the uncertainties in the interpretation of the RSS data, two effects need to be considered. First, the total number density derived from the refractivity depends on the composition through equation (1).  $CH_4$  has the highest molecular refractivity and Ar the lowest; therefore, the models with maximum number density will be achieved with the smallest possible abundance of  $CH_4$  and the largest possible abundance of Ar. Second, the mass density is related to the number density by the molecular weights of the constituents. Because  $CH_4$  has the smallest mass and Ar the largest, the maximum mass density is again achieved with the smallest possible  $CH_4$  abundance and the largest possible Ar abundance. Also, the RSS data, by defining the variation of number density with altitude, determine the ratio of temperature to mean molecular mass, *Tim.* Therefore, the models with the largest  $CH_4$  abundance will have the lowest temperatures as well as the smallest mass density. Conversely, models with the smallest  $CH_4$  abundance will have the largest possible  $CH_4$  is condensible. This is discussed further below.

Strobel et al. (1993) have determined the Ar mole fraction to be less than 10% and the  $CH_4$  mole fraction just above the tropopause to be greater than 2.6%. We adopt values of 10% and 1% for Ar and  $CH_4$ , respectively, to be conservative. Using these values, we calculate a maximum mass density model from the RSS occultation data. The mole fraction of  $CH_4$  in the troposphere is taken to be constant because at this low abundance it will not condense.

Choosing a minimum mass density model is more difficult. As mentioned above, to minimise the mass density inferred from the RSS data requires using the minimum abundance of Ar and maximum abundance of  $CH_4$ . We find that it is difficult to fit the UVS and IRIS data simultaneously with  $CH_4$  mole fractions greater than 5% and adopt this value for the  $CH_4$  mole fraction in the stratosphere. Assuming no argon, we find that a  $CH_4$  abundance near the surface greater than 10% implies a super-adiabatic temperature profile at the surface, relative to the dry adiabat. Therefore, the  $CH_4$  profile adopted for the minimum model has a mole fraction of 10% at the surface.  $CH_4$  continues with this relative abundance until the condensation point is reached. The  $CH_4$  distribution then decreases with increasing altitude (and decreasing temperature) until a mole fraction of 5% is reached. The  $CH_4$  mole fraction then remains constant until diffusive equilibrium takes effect near 600 km. The  $CH_4$  distribution in this model is supersaturated in the troposphere and the abundance in the stratosphere is larger than implied by the vapour pressure value at the tropopause. This situation is unlikely but this choice was made because it is our intent to construct a model with the maximum abundance of  $CH_4$  (and minimum mass density). The minimum model contains no argon.

Temporal and/or spatial variations in atmospheric structure are accounted for by perturbing the temperature profiles of the maximum and minimum models just described. We add (to the maximum model) and subtract (from the minimum model) a temperature difference that varies with altitude. Below 200 km we use values for the temperature difference from the LR report, which are reproduced in Table 2. These values are obtained by considering known latitudinal temperature variations in the stratosphere and plausible variations in the troposphere. The temperature perturbations at altitudes above 200 km are chosen with guidance from physically-based thermal structure calculations. Using the calculations described in YelIe (1991), we construct temperatures are obtained with no aerosol heating and the warmest when the aerosol heating rate corresponds to 30% of the solar flux absorbed in the upper atmosphere. These temperature profiles differ from the recommended temperature profile by roughly 30 K; therefore, we adopt this as the uncertainty in the upper atmospheric temperature profile.

After constructing new maximum and minimum temperature profiles, we integrated the hydrostatic equilibrium equation upward from the surface, assuming that the composition is the same

as in the unperturbed maximum and minimum models. This integration requires a lower boundary condition on surface pressure.

Large temporal variations in surface pressure on Titan are not expected because the time constants for changing the structure of the lower atmosphere or ocean (if it exists) are very long. There may be variations in surface pressure due to topography and/or weather systems. Topography at the 1 km level would produce variations in surface pressure on the order of 2%. Variations in surface pressure due to weather systems are difficult to predict because we know so little about weather on Titan. On Earth, weather systems produce variations of surface pressure of roughly 5 % and we adopt this as an estimate of the surface pressure uncertainty on Titan. Titan's weather is likely to be less intense than Earth's, so this assumption is conservative. We include the uncertainty in surface pressure and topography in the models by decreasing (increasing) the surface pressure by 5% for the minimum (maximum) models. The uncertainty in composition also causes an uncertainty in surface pressure by altering the density and mean molecular mass of the atmosphere. Both uncertainties are incorporated in the models. The minimum model has a surface pressure of 1.35 bar and the maximum model a surface pressure of 1.61 bar.

The temperature uncertainty, DT grows with altitude in Titan's atmosphere. Near the surface, where DT is fairly small, the uncertainties in composition dominate the error budget. The uncertainty in the upper atmospheric structure, however, is totally dominated by the uncertainty in temperature. Therefore, when constructing the maximum and minimum models, we neglect the possibility of further changes in composition and use the same parameters to calculate diffusive separation that were used in the recommended model. Specifically, we used equations (3) and (4) to calculate the CH<sub>4</sub> and Ar mole fractions, with the parameters listed in Table 1.

The maximum and minimum profiles constructed in this fashion represent physically possible, if implausible, atmospheres. They have well-defined compositions and the atmospheric parameters of pressure, temperature and density are related in the proper way by the equation of state and the hydrostatic equilibrium equation. The temperature profiles are everywhere subadiabatic, but  $CH_4$  is supersaturated in limited regions in both the recommended model and the minimum model.

We close this report with some remarks on the meaning of the maximum and minimum models.

For the purposes of an engineering reliability study, it is useful to assign formal probabilities to the range of model atmospheres presented in this report. Unfortunately, the models presented here are not easily identified with members of a statistical ensemble and therefore assignment of formal probabilities is more guesswork than science or engineering. The maximum and minimum models are based on physical consideration of atmospheric processes but we have made conservative assumptions. To construct the maximum and minimum models we assumed that the uncertainties in temperature and composition combine to maximise the distance from the recommended model. It is probably more realistic to assume that these uncertainties may partially offset each other. Moreover, we have assumed a large value of AT of the same sign at each altitude in the maximum and minimum models. Realistic spatial and temporal variations are more likely to result from changes in shape of the heating profile, causing larger temperatures at one level and lower temperatures at another. Therefore, the maximum and minimum models represent extreme cases and it is highly likely that Titan's atmosphere as measured by Huygens will fall between these extremes. However, we know of no justifiable way to assign a formal probability to this statement.

Table 1. Parameters used in the construction of the compositional profiles for the recommended, minimum and maximum models.

Parameter	Rec.	Min.	Max.
k	0.625	0.500	0.100
A1	0.240	0.009	0.044
A2	0.006	0.001	0.006
$Z_h$	1050.0	830.0	1100.0

 

 Table 2. Parameters used in the construction of the temperature profiles for the recommended, minimum and maximum models.

Pressure ( <b>m</b> bar)	DT(K)
1.5 x 10 <sup>6</sup>	3
$1.5 \ge 10^2$	3
300.0	20
30.0	30

## 4. Summary

Table 3. Recommended Yelle model for Titan's atmosphere. CH<sub>4</sub> 3%, Ar 2%, N<sub>2</sub> 95%, mean mass 27.81, T(1) = 1750, T(2) = 135.0, T(3) = 175.0,  $\kappa = 0.625$ , A<sub>1</sub> = 0.024, A<sub>2</sub> = 0.006, A<sub>3</sub> = 0.020, Z<sub>h</sub> = 10500.

Z	Nu	mber Den	sities (cm	5	Mats	Pressure	Temp	F	Z	Number Densities (cm <sup>3</sup> )		Mast	Pressure	Temp	F		
(km)	Total	N	CH	Ar	(em/cm <sup>2</sup> )	(erg/cm)	(K)	e	(km)	Total	N	CH	Ar	(em/cm <sup>3</sup> )	(erg/cm <sup>2</sup> )	(K)	· · ·
		2	4								2	4	120000				
1300.0	.229E+09	.197E+09	.299E+08	.144E+07	.100E-13	.552E-05	175.00	.000E+00	890.0	.389E+11	.367E HI	.164E i 10	.584E+09	.178E 11	.935E 03	174.29	.000E+00
1295.0	.241E+09	.209E+09	_310E+08	.154E+07	.106E-13	.583E-05	175.00	.000E+00	885.0	,418E+11	.394E+II	.175E+10	.632E+09	.192E-0	.100E-02	174.08	000E+00
1290.0	.255E+09	221E+09	.322E+08	.J65E+07	.II2E-I3	616E-05	175.00	.000E+00	880.0	450E+11	424E+U	.187E+H	.684E+09	.206E-11	.108E-02	173.85	.000E+00
1285.0	.269E+09	.234E+09	.334E+08	.177E+07	.119E-13	651E-05	175.00	1000E+00	875.0	.484E+11	.457E+U	.1996+10	.741E+09	.222E-U	.116E-02	173.58	D00E+00
1280.0	.285E+09	.248E+09	.347E+08	.189E+07	.126E-13	.687E-05	175.00	.000E+00	870.0	.521E+11	.492E+11	.213E+10	1900E+09	.239E-11	125E-02	173.30	000000000
1275.0	.301E+09	.263E+09	.360E+08	203E+07	133E-13	.727E-05	175.00	D00E+00	865,0	362E+11	572E+11	244E+10	.87CE+09	-256E-0	14/E-02	172.98	000E+00
1265.0	1162+00	2705109	3982 109	2735-407	140E 13	9032-05	125.00	000E+00	8550	653E+11	617E+11	2616+10	100E+10	300E-11	155E-02	172.28	000E+00
1260.0	356E+09	313E+09	403E+08	249E+07	158E-13	859E-05	175.00	.000E+00	8500	205E+11	666E+11	.280E+10	.ILE+10	.323E-II	.167E-02	171.90	.000E+00
1255.0	376E+09	332E+09	49E+08	267E+07	167E-13	908E-05	175.00	000E+00	8450	.761E+11	719E+11	.300E+10	.12IE+10	.349E-II	.180E-02	171.49	.000E+00
1250.0	.398E+09	351E+09	.435E+08	.286E+07	.177E-13	96IE-05	175.00	.000E+00	840.0	.822E+11	.777E+11	.322E+10	.13IE+10	.377E-II	.194E-02	171.05	.000E+03
1245.0	.421E+09	.373E+09	.453E+08	.307E+07	.187E-13	.102E-04	175.00	.000E+00	835.0	.888E+11	.839E+11	.345E+10	143E+10	.408E-11	.209E-02	170.60	.000E+00
1240.0	.446E+09	.395E+09	.47IE+09	.329E+07	.198E-13	.108E-04	175.00	.000E+00	830.0	.961E+11	.908E I II	.37IE+10	.155E+10	.441E 11	.2268-02	170.12	.000E+00
1235.0	.472E+09	.419E+09	.490E+08	.353E+07	.210E-13	.114E-04	175.00	.000E+00	825.0	.104E+12	.983E+11	.399E+10	.169E+10	.478E-11	.243E-02	109.01	.000E+00
1230.0	.499E+09	.445E+09	.50E+08	.378E+07	.222E-13	.121E-04	175.00	,000E+00	820.0	.113E+12	.106E+12	.429E+10	.185E+30	.517E-11	260E-02	169.59	00000+00
1225.0	.529E+09	A72E+09	.53IE+08	4068+07	.236E-13	.L3E-04	1/5.00	000E+00	815.0	(12ZE+12 (13E+13	105E+12	.402E+10	2000+10	.300E-II	3/02-01	108.33	100E+00
1220.0	.300E+09	.501E+09	.553E-+06	4352+07	-2506-13	1356-04	175.00	000E+00	BRED	132E+12	123E+12 126E+12	498E+10	200E+W	550E 11	33/6-02	167.30	000E+00
1215.0	.393E+09 6307±09	55/E+09	-515E+06	.40/E+0/ 50/E+07	2815-13	1575-04	175.00	000E+00	8000	156E+12	.130E+12	580E+10	259E+10	716E-11	354E-02	166.79	.000E+00
1205.0	6665+09	504E+04	625E+08	\$18E+07	298F-13	161E-04	175.00	000E+00	7950	160E+12	360E+12	.626E+10	283E+10	.778E-11	.38#E-02	166.16	.000E+00
	inners ( sec					-10111 1-1											
1200.0	.706E+09	635E+09	.651E+08	.577E+07	316E-13	.171E-04	175.00	.000E+00	790.0	384E+12	174E+12	677E+10	.309E+10	.845E-11	.420E-02	165.51	.000E+00
1195.0	.749E+09	.675E+09	.679E+08	.620E+07	.335E-13	.181E-04	175.00	.000E+00	785.0	.200E+12	.189E+12	.733E+10	.337E+10	.920E-11	.455E-02	164.85	.000E+00
1190.0	.794E+09	.717E+09	.708E+08	.665E+07	.356E-13	.192E-04	175.01	.000E+00	780.0	.218E+12	.206E+12	.793E+10	.369E+10	.100E-10	.493E-02	164.17	.000E+00
1185.0	.842E+09	.76IE+09	,739E+08	.714E+07	.378E-13	203E-04	175.01	.000E+00	715.0	.237E+12	.225E+12	.860E+10	.403E+10	.109E-10	.535E-02	163.47	000E+00
1180.0	_894E+09	.809E+09	.771E+08	.767E+07	.401E-13	.216E-04	175.0)	.000E+00	770.0	.259E+12	.245E+12	.932E   10	.443E   10	J19E-10	.58E 02	162.75	000E+00
875.0	.9488.+09	.859E+09	.809E+08	824E+07	.426E-13	229E-04	175.00	000E+00	7650	.282E+12	2078+12	1012+11	4040.110	1419.10	681E-02	162.52	0005+00
II AUD	.101E+H0	.9EE+09	.SHE+08	285E+0/	.452E-13	243E-04	105,07	000E+00	7660	308E+12	2926+12	11000 + 11	5010 ± 10	14428-10	745E-01	160.51	000E+00
1003.0	10/E+10	.9/IE+09	.819E+08	(951E+0)	.480E-13	238E-04	10.00	000E+00	2600	350E+12 368E±12	348E ±13	1306-11	638E110	100E-10	806.02	159.74	000E+00
1050.0	110E+10	100E+10	-91615+06 0601E±08	1025+08	S47E-13	294E-04	175.00	000E+00	7450	402E+12	38IE +12	142E+11	20(E+10	185E-10	881E-02	158.95	000E+00
8330	.1200.710	LINCTIC	190011908	JIMETOO		140410-04	110000	10012 1000	1450	. These is the	Contract of the	Strate i il	indite i pe	100200-00	and the second		
1150.0	.128E+10	.117E+10	.100E+09	.18E+08	576E-13	.309E-04	175.00	.000E+00	7400	.441E+12	.418E+12	.154E+11	.77IE+10	.203E-10	.962E-02	158.15	.000E+00
045.0	.136E+10	.124E+10	.105E+09	.127E+08	.612E-13	.328E-04	175.00	.000E+00	735.0	.483E+12	.458E+12	.169E+11	.848E+10	.222E-10	.105E-01	157.33	000E+00
1140.0	.144E+10	.132E+10	.10E+09	.136E+08	.651E-13	.349E-04	175.00	000E+00	7300	.530E+12	_502E+12	.184E+11	.933E+10	.244E-10	.114E-01	156.51	000E+00
1135.0	.153E+10	.140E+10	.115E+09	.147E+08	692E-13	.370E-04	175.00	.000E+00	7250	.582E+12	.551E+12	.201E+11	.103E+11	_268E-10	.125E-01	155.68	000E+00
1130.0	.163E+10	,149E+10	.120E+09	.158E+08	.736E I3	.394E 04	175.00	1000E+00	7200	.639E+12	.605E+12	.220E+H	.113E+11	_294E-10	.137E-01	154.84	DODE+00
1125.0	.173E+10	.159E+10	.126E+09	.169E+08	.783E-13	.419E-04	175.00	.000E+00	715.0	.703E+12	,666E+12	.241E+11	.125E+11	_324E-10	.149E-00	153.99	000E+00
1120.0	.184E+10	.169E+10	.132E+09	.182E+08	833E-13	.445E-04	175.00	.000E+00	710.0	.773E+12	.733E+12	.265E+11	-138E+10	_356E-10	.363E-00	153.34	000E+00
1115.0	.196E+10	.180E+10	.138E+09	.196E+08	886E-13	.473E-04	175.00	.000E+00	7050	.8528+12	80/E+I2	2906+11	1538-11	_392E-10	1068-00	151.42	000E+00
1000	.209E+10	192E+10	1435-149	201E+08	9435-13	.304E-04	175.00	000E+00	6050	104E+12	0925+12	359E+11	107E ±11	A77E-10	215E-01	150.56	000E+00
105.0	.222E+10	.204E+10	DZETUS	2276708	.ROUE-12	3306-04	175.00	10002-000	0950	.1040+15	19060 116	30016711	101010111	.41712-10		Done.	10000
1000	2368-16	218E+10	160E+09	2147+08	107E-12	520E-04	175.00	000E+00	6900	114E+13	108E+13	386E+11	.207E+II	.52TE-10	.236E-01	149.70	.000E+00
1095.0	.250E+10	232E+10	.167E+09	.263E+08	.114E-12	.607E-04	175.00	.000E+00	6850	.126E+13	.120E+13	.425E+11	.229E+II	.582E-10	.260E-01	:48.84	.000E+00
1090.0	268E+10	247E+10	125E+09	283E+08	121E-12	646E-04	175.00	.000E+00	680.0	.140E+13	.133E+13	.468E+11	.254E+II	.644E-10	.286E-01	147.99	.000E+00
1085.0	.285E+10	.263E+10	.185E+09	.304E+08	.129E-12	.688E-04	175.00	.000E+00	675.0	.155E+13	.147E+13	.517E+11	.282E+II	713E-10	.314E-01	147.14	.000E+00
1090.0	.303E+10	.281E+10	194E+09	.3288+08	139E-12	733E-04	175.00	.000E+00	6700	.172E+13	.163E+13	.57IE+11	.314E+11	791E-10	.346E-01	146.29	.000E+00
1075.0	.323E+10	299E+10	.204E+09	.353E+08	.147E-12	.781E-04	175.00	.000E+00	665.0	.190E+13	.180E+13	.631E+11	.349E+II	877E-10	.382E-0	145,46	.000E+00
1070.0	.344E+10	'315R+10	.2HE+09	,380E+08	.156E 12	.832E 04	175.00	.000±±000.	660.0	211E+13	,200E+13	.699E+11	.388E+8	973E-10	422E-0	144.64	000E+00
1065.0	.367E+10	_340E+10	.225E+09	.409E+08	.167E-12	.886E-04	175.00	.000E+00	655.0	_235E+13	.223E+13	.774E+11	.432E+11	.108E-09	.406E-01	143.83	000E+00
1060.0	.391E+10	_363E+10	.237E+09	.440E+08	_178E-12	.945E-04	175,00	.000E+00	6500	.261E+13	.2476:+13	358E+11	.4826 11	120E-09	.50E 01	142.22	000E+00
1055.0	.417E+10	_387E-+10	.249E+09	.474E+08	.190E-12	.IDIE-03	1/5/00	1000E+00	645.0	_290E+13	.2/36+13	3316+11	-33/E70	.1346.409	.5 AUE-06	146.67	MAR TUS
10500	4450+10	4137.1.0	2620 400	SHELOR	2025-12	107E-03	175.00	000E+00	6400	3238+13	3068+13	106E+12	500E+11	149E-09	63E-01	141.52	.000E+00
10450	474E+10	4136 + 10	2268-00	550E+08	216E-12	IISE-03	175.00	800E+00	6350	360E+13	34IE+13	117E+12	669E+II	166E-09	.699E-01	140.79	.000E+00
1040.0	506E+10	47(E+10	29/E+09	503E+08	230E-12	.122E-03	175.00	000E+00	6300	.401E+13	.38IE+13	131E+12	.748E+11	.185E-09	.776E-01	140.09	.000E+00
1035.0	.540E+10	_503E+10	.307E+09	.639E+08	.246E-12	.130E-03	175.00	.000E+00	625.0	.448E+13	.425E+13	.145E+12	.836E+11	.206E-09	.86(E-0)	139.43	000E+00
1030.0	.576E+10	.537E+10	.323E+09	.688E+08	.262E-12	.139E-03	175.00	.000E+00	6200	.500E+13	.474E+13	.162E+12	.935E+II	.230E-09	.957E-01	138.79	.000E+00
1025.0	.615E+10	.574E+10	.34IE+09	.742E+08	.280E-12	.149E-03	175.00	.000E+00	615.0	.558E+13	_530E+13	.180E+12	.105E+12	.257E-09	.106E+00	138.19	000E+00
1020.0	.657E+10	.613E+10	.359E+09	.800E+08	299E-12	159E-03	175.00	000E+00	610.0	.624E+13	_592E+13	.201E+12	.II7E+12	_287E-09	.118E+00	137.64	000E+00
1015.0	.701E+10	.655E+10	.379E+09	.862E+08	.320E-12	.169E-03	175:00	.000E+00	605.0	.697E+13	.662E+13	.224E+12	.13E+12	.321E-09	.132E+00	137.12	0000000000
1010.0	.749E+10	.699E+10	.400E+09	.929E+08	_341E-12	.181E-03	175.00	.000E+00	6000	380E+13	.7406+13	250E+12	.147E+12	_359E-09	.147E+00	136.05	0008+00
1005.0	300E+10	.745E+10	.423E+09	.100E+09	365E-12	1936-03	175.00	100E+00	393.0	B72E+13	10200 +13	198+12	10012 +12	.40212-09	1046+00	130.24	0005100
10000	-	90007.4.10	4470-00	1097.4.10	3000.12	2068-03	175.00	000E+00	5900	036E+13	927E+13	312E+12	185E+12	450E-00	183E+00	13582	000E+00
995.0	WIRE+W	855E+10	407E+09	1065.409	4175-12	721E-03	175.00	000E+00	5850	109E+14	.104E+14	348E+12	.207E+12	.504E-09	.204E+00	135.57	.000E+00
990.0	976E+10	914E+10	499E+09	126E+09	4468-12	236E-03	175.00	.000E+00	580.0	122E+14	.116E+14	389E+12	232E+12	.564E-09	.228E+00	135.33	.000E+00
985.0	.104E+11	.978E+1)	.527E+09	135E+09	477E-12	.252E-03	175.00	.000E+00	575.0	.137E+14	.130E+14	A35E+12	.261E+12	631E-09	.255E+00	135.15	.000E+00
980.0	.112E+11	.105E+11	-558E+09	.146E+09	.510E-12	.270E-03	175.00	.000E+00	570.0	.153E+14	.146E+14	,486E+12	.292E+12	J07E-09	.286E+00	135.04	.000E+00
975.0	.119E+11	.112E+1	.590E+09	.158E+09	.5458-12	.288E-03	175.00	.000E+00	565.0	.172E+14	.163E+14	.543E+12	.328E+12	.79IE-09	.320E+00	135.00	.000E+00
970.0	.128E+11	_120E+1I	.625E+09	.170E+09	.584E-12	.308E-03	175.00	.000E+00	560.0	.192E+14	.182E+14	.607E+12	_367E+12	.886E-09	.358E+00	135.05	.000E+00
965.0	.B7E+11	.128E+11	,662E+09	.183E+09	.625E-12	.330E-03	175.00	.000E+00	555.0	.215E+14	.204E+14	.678E+12	.411E+12	.991E-09	.40(E+0)	135.22	.000E+00
960.0	.146E+11	.137E+11	.701E+09	.198E+09	.669E-12	.353E-03	175.00	.000E+00	550.0	240E+14	278E+14	756E+12	.460E+12	.111E-08	.449E+00	135.49	000E+00
955.0	.BTE+H	.147E+1	.M3E+09	.ZI4E+09	.716E-12	-378E-03	05.00	.000E+00	545.0	.208E+14	.2358+14	543E+12	-30E+12	1248-08	.50E+00	133,83	100E+00
040.0	ISEE +11	1970 - 1	372+00	2110-100	7678.12	405E-03	175.00	(00E+00	5400	299F+14	2848 +14	940E+12	5%E+D	138E-08	.561E+40	136.32	.000E+00
9450	180E+11	169E + 1	.835E+09	249E+09	821E-12	.434E-03	175.00	.000E+00	5350	3346+14	31712+14	105E+13	643E+12	154E-08	.63IE+00	136.87	.000E+00
940.0	.192E+11	.18/E+11	.886E+09	_269E+09	880E-12	464E-03	175.00	.000E+00	530.0	372E+14	.353E+14	.117E+13	.7BE+12	172E-08	.706E+00	137.50	.000E+00
9350	206E+1	.194E+11	.940E+09	.290E+09	.9436-12	.498E-03	175.00	_000E+00	525.0	.415E+14	.394E+14	130E+13	.800E+12	.191E-08	.79(E+00	138.22	.000E+00
930.0	.22(E+1)	208E+1	.998E+09	.313E+09	.101E-11	_533E-03	175.00	.000E+000	520.0	.462E+14	.438E+14	144E+13	.892E+12	213E-08	.885E+00	139.01	.000E+00
925.0	.237E+11	.223E+II	.106E+10	.338E+09	.1082-11	.572E-03	175.00	.000E+00	\$15.0	.513E+14	.487E+14	.160E+13	.993E+12	.237E-08	.99IE+00	139.86	.000E+00
920.0	.254E+11	.239E+II	.113E+10	.365E+09	.116E-11	.613E-03	174.98	.000E+00	510.0	.571E+14	.542E+14	.178E+13	.1DE+13	.263E-08	.IIIE+0I	140.78	,000E+00
915.0	.272E+11	.256E+II	.120E+10	.395E+09	.1258-11	657E-03	174.94	.000E+00	505.0	634E+14	.602E+14	.197E+13	.123E+13	.292E-08	.124E+0	141.75	.000E+00
910.0	.292E+1	.275E+#	.127E+10	.427E+09	,1348-11	.705E-03	174.85	000E+00	500.0	.703E+14	668E+14	.218E+13	150E+B	.324E-08	.159E+0	142.78	000E+00
905.0	_314E+11	.295E+1	.136E+10	.401E+09	.1448-11	.008-03	174.76	100E+00	495.0	.780E+14	.741E+14	_242E+13	,1528-15	200E-08	1000-40	14385	ANUE +00
9000	33754.11	3778+1	144E+10	4998+09	1547-11	8UE-03	174.63	000E+00	490.0	864E+14	.821E+14	268E+13	.168E+13	399E-08	.173E+0	144.95	.000E+00
895.0	.362E ( 1)	.34IE   1	.154E 1 10	_539E+09	.1668 11	\$71E-03	174.48	.000E+00							12	ontinued of	m mest prope
1	19-21-22-22				CCC			A CONTRACTOR OF THE									

Table 3. (Continued).

																1.1	-
Z	Nu	mber Den	sities (cm	3)	Mass	Pressure	Temp	F	7	N	other Des	sities less	3	Maco	Pressure	Tomo	F
Anni	Treat	N	CH		land land	Come land	18%	¢			whiter Lien	annes (cm	1	3	3.	nemp	° c
iventy	Torett	142	CH4	Ar	(gm/cm)	(erg.cm)	(v)		(km)	Total	N <sub>2</sub>	CH	Ar	(gm/cm)	(erg/cm <sup>*</sup> )	(K)	
Sugar		Constanting of the	and the second second	Contraction Constra	3.337.5.114.2	Landa State	12.032520	Constant Procession of the	1	10.000			S	Constrained.	and and the second	-	1000000
485.0	.957E+14	.909E+14	.296E+I3	.186E+13	.442E-08	.193E+0i	146.10	.000E+00	150.0	.10E+18	.104E+18	.329E+16	.219E+16	.506E-05	.245E+04	161.92	.100E-04
480.0	.106E+15	.101E+15	.328E+I3	.205E+13	.489E-08	.215E+0(	147.28	.000E+00	148.0	.116E+18	.110E+18	.347E+16	.23(E+16	533E-05	.257E+04	161.50	100E-04
475.0	.II7E+15	.IIIE+15	.362E+13	.228E+15	.541E-08	.240E+08	148.48	000E+00	146.0	.122E+18	.116E+18	.367E+16	245E+16	565E-05	271E+04	160.26	100E-04
4700	130E+15	1238+15	400F+13	253E+13	\$98E-08	268E+08	140.70	000E+00	144.0	1785 +18	1226+18	385E+16	257E+16	5978-05	285E+04	160.79	100E-04
465.0	143E+15	116E+15	ANE-13	2800-113	6600.09	2095 +/8	150.03	0005+00	117.0	13612 + 19	1205-19	ADOF 1.16	2726+16	6701.05	2006-104	160 74	TOOF OA
460.0	1436+12	-190E+15	4416-13	.280E +15	20002-08	2386+01	150.95	000E+00	144.0	13013 118	1296 + 18	.409E+16	2720+10	6296-05	.500E+04	129.30	1006-04
4600	1386+13	-BOE+15	.48/8.+(3	.309E+13	.729E-08	-332E+0I	152.18	000E+00	140/0	1448.+18	1378+18	.432E+95	.2888+10	000E-00	3BE+04	158.55	.2005-04
400.0	4746+15	-100E+15	.537E+13	.341E+13	305E-08	_369E+0I	153.43	D00E+00	138.0	.152E+18	_144E+18	,436E+16	.3042+36	.702E-05	.332E+04	158.25	.200E-04
450.0	.192E+15	_183E+15	.59IE-13	.377E+13	.888E-08	,40E+01	154.69	000E+00	136.0	.16IE+18	153E+18	.483E+16	_322E+16	.743E-05	_351E+04	157.45	200E-04
445.0	.212E+15	.201E+15	.652E+13	,416E+13	.979E-08	.457E+0I	155.94	.000E+00	134.0	.170E+18	.16IE+18	.509E+16	.340E+16	784E-05	.368E+04	157,18	.200E-04
440.0	.234E+15	.222E+15	.718E+13	.458E+13	.108E-07	.507E+00	157.19	000E+00	132.0	.180E+18	.171E+18	.539E+16	.359E+16	829E-05	_389E+04	156.51	.200E-04
-100020																	
435.0	258E+15	245E+15	290E-13	505E+13	195.07	563E±08	158.44	000E+00	130.0	100F 418	1805+18	560F116	170E±16	\$75E-05	4005+04	156 34	200E-04
4300	2848+15	260E+15	8695-13	557E+13	1118-07	6755+0	150.44	0005+00	128.0	70UE +10	10002 110	SOME + 16	10010+16	03/02-05	4312-404	155.11	2005-04
475.0	2016 + 15	32161.15	00702113	61481113	DAE 07	ADDET OF	15009	DODE 100	156.0	2016 110	1915 110	5420114	4036110	09002-00	4512 104	162.00	2005-04
4230	3126+13	.2976+15	.9376+13	.01912+1.5	144E-07	1094E+0E	IDUAS	D00E+00	120.0	.2148.+18	-2048+18	D43E+10	.9288+10	-989E-00	.4336.404	133,80	2006-04
420.0	,344E+15	.327E+15	1K2E+14	.676E+13	.159E 07	.769E+01	162.08	000E+00	124.0	.227E+18	216E+18	081E+16	.4548+16	I05E-04	.480E+04	153.10	300E-04
415.0	.378E+15	.359E+15	_D6E+14	.745E+13	175E-07	A2254	163.25	1000E+00	122.0	.242E+18	_230E+18	.726E+16	.484E+16	_H2E-04	.505E+04	151.73	.300E-04
410.0	.416E+15	.396E+15	.127E+14	.820E+13	.192E-07	.945E+0I	164.40	.000E+00	120.0	.257E+18	_244E+18	.770E+16	.513E+16	.118E-04	.535E+04	151.00	_300E-04
405.0	.458E+15	.435E+15	.140E+14	.902E+13	.2IIE-07	.105E+02	165.52	.000E+00	118.0	.272E+18	.259E+18	.817E+16	.545E+16	126E-04	.565E+04	150.28	.300E-04
400.0	.504E+15	.479E+15	154E+14	993E+13	233E-07	116E+02	166.61	000E+00	16.0	289E+18	275E+18	868E+16	579F+16	134E-04	597E+04	149.6	.40IE-04
395.0	.555E+15	.527E+15	.169E+14	.109E+14	.256E-07	.128E+02	167.66	000E+00	114.0	.307E+18	.292E+18	.921E+16	.614E+16	142E-04	.63IE+04	149.01	.401E-04
390.0	.610E+15	.579E+15	186E+14	120E+14	28IE-07	142E+02	168.68	000E+00	82.0	327E+18	310E+18	980E+16	654E+16	151E-04	668E+04	148.05	401E-04
				100 0 00 10 1	a character of	11 18 18 1 1 18			and the	100.00.00							
1950	6TIE +15	63784.15	2045-14	1375.414	1005.02	15784.02	16066	0005-100	100	3486.119	3305.18	104E-17	605E.L.14	1608.04	TISELOA	147.31	4015.04
180.0	7395.415	2010-16	1140.14	1460.014	3412 07	1748 + 02	130.60	0002+00	108.0	3600.112	1510-10	1110 - 12	73902400	1305.01	7488-04	116.73	400E 04
2000	3360+D	CITIZIO.	04770-04	Sect des	.341E-07	10000.000	17000	000E+00	108.0	3096 18	-331E+18	there in	206510	.1706-04	34457404	140.73	4000 04
375.0	312E+13	.//IE+15	.24/6+14	.100E+14	.3/SE-07	.072E+02	1/1.49	DUDE+00	106.0	.393E+18	.37315十副	118E+17	80E+16	.181E-04	.192E+04	145.98	499E-04
370.0	.894E+15	.849E+15	.272E+14	.177E+14	.412E-07	.213E+02	172.33	000E+00	104.0	.421E+88	.400E+18	.126E+17	.841E+16	.194E-04	.838E+04	144.47	.499E-04
365.0	.983E+15	.934E+15	.299E+14	.194E+14	.454E-07	.235E+02	173.12	000E+00	102.0	.449E+18	.427E+18	.135E+17	.898E+16	.207E-04	.889E+04	143.37	600E-04
360.0	.108E+16	_103E+16	.329E+14	.214E+14	.500E-07	.260E+02	173.85	.000E+00	100.0	.481E+18	.457E+18	.144E+17	.962E+16	_222E-04	.943E+04	142.06	600E-04
355.0	JI9E+16	.III3E+16	.362E+14	.236E+14	.550E-07	.287E+02	174.53	.000E+00	98.0	.5I4E+I8	.489E+J8	.154E+17	.J03E+17	.237E-04	.100E+05	140.91	700E-04
350.0	.131E+16	125E+16	.399E+14	.260E+14	606E-07	.317E+02	175.15	000E+00	96.0	55(E+18	.523E+18	.165E+17	.110E+17	2548-04	.106E+05	139.70	800E-04
345.0	145E+16	137E+16	439E+14	287E+14	668E-07	351E+02	125.71	000E+00	94.0	592E+18	563E+18	178E+17	.118E+17	273E-04	.1I3E+05	138.05	800E-04
3400	159E+16	151E+16	484F+14	316F+14	736E-07	3997+02	176.21	000E+00	92.0	639E+18	607E+18	192E+17	128E+17	295E-04	120E+05	136.15	900E-04
				10100 111	areas or	100000 7 000										in some	
2250	1760 + 16	1670.116	6338-14	2408.144	91212 02	1208.102	196.65	00000.000	200	6960 119	6610 + 10	1045 - 17	1215-17	3178-04	1100.405	114 00	1002.01
333/0	1045 + 10	10/10/10	.53.31.+24		B1217-177	4296 112	1000.9	0005+00	90.0	.10001-10	A326+18	2006+11	1375+17	3305-04	120151105	124.90	HOE 03
330.0	1945+16	_184E+10	388E+94	.385E+14	/895E-07	.4/48+08	17/003	000E+00	0.58	J.DE.+18	,098E+18	.220E+1	,降(医+1)	-3398-04	-130E+03	134.20	.HDE-03
3250	.214E+16	.203E+16	.649E+14	.425E+I4	.988E-07	.524E+02	177.36	.000E+00	86.0	.795E+18	.755E+18	.238E+17	.159E+17	.367E-04	.145E+05	132.19	.1208-03
320.0	.236E+16	.225E+16	.716E+14	.469E+14	.109E-06	.580E+02	17763	.000E+00	84.0	.866E+18	,823E+18	.260E+17	.173E+17	.400E-04	.155E+05	129.47	.140E-03
315.0	.26IE+16	.248E+16	.791E+14	.519E+14	.121E-06	.541E+02	177.85	.000E+00	82.0	.948E+18	.900E+18	.284E+17	.190E+17	.438E-04	.165E+05	126.41	.150E-03
310.0	.289E+16	.274E+16	874E+14	573E+14	133E-06	710E+02	178.01	000E+00	80.0	.104E+19	.986E+18	311E+17	.208E+17	479E-04	.177E+05	123.61	.180E-03
305.0	319E+16	303E+16	OSSF 414	634E+14	147E-06	785E 4/12	178.13	000E+00	7843	114E+19	1096+19	143E+17	778E+17	577E-04	1908-405	120.42	200E-03
1000	3546-16	136E+16	107E-15	202E+14	1672 06	2005 + 02	176.10	000E+00	76.0	12682-130	1102.1.10	3778+17	2526+17	5818-04	2048+05	107.51	230E-03
205.0	3022 116	2002110	10712-15	199000 114	10012-00	0622102	176.12	00000100	240	120/2 1 10	1120710	4970.17	12310 1 17	641E 04	2226 105	11.0 65	220E 02
2900	.392E+10	.3/2E+10	.118E+15	./JSE+14	-BALE-00	.903E+02	1/8.41	000E+00	34.0	.1.99E+19	.132E+19	.407E+17	.2/82+1/	.0412-04	.2208+05	199.00	2706-00
2900	.434E+10	.41211+16	.DIE+15	_862E+14	_200E-06	.107E+03	17E.17	000E+00	72.0	.1501:+19	_D48E+19	.469E+1/	30E+1/	.721E-04	.23VE+05	109/90	330E-03
1.5.50									1225						S		- Secondaria
285.0	.481E+16	.457E+16	.145E-15	.956E+14	.222E-06	.118E+03	17809	000E+00	700	.179E+19	.170E+19	537E+17	358E+17	827E-04	.257E+05	103.94	.410E-03
280.0	.534E+16	.507E+16	.161E+15	.106E+15	_246E-06	.131E+03	172.97	.000E+00	68.0	.206E+19	.196E+19	.618E+17	.412E+17	.951E-04	.280E+05	98.37	.520E-03
275.0	.593E+16	.563E+16	.179E-15	.118E+15	.274E-06	.145E+03	177.80	.000E+00	66.0	.243E+19	.23IE+19	.729E+17	.486E+17	.II2E-03	.305E+05	91.37	.700E-03
270.0	.659E+16	.626E+16	.199E-15	.13IE+15	304E-06	.161E+03	177.58	000E+00	64.0	.289E+19	.275E+19	B67E+17	.578E+17	.1338-03	.338E+05	84.71	.950E-03
2650	737E+16	606E±16	221E-15	1455-115	33917-06	1798+03	177 32	000E+00	62.0	3.017.1.10	3745-10	107F+18	68IE±17	157E-03	375E405	70.80	1248-02
2600	\$15E + 16	274E186	246E115	167E+15	376E.06	100E+01	17202	000E+00	600	3065 + 10	376E + 10	1108+15	2016+17	1832.03	419E+05	36.95	154E.02
3650	DORE 116	DODE 16	224011415	1026 415	1005.06	2215 - 02	17102	00000100	600	45782430	4362 110	1196 + 10	AND ALL	1000-00	4701-105	70.07	1980 02
2550	908E+10	1802E+10	2048+15	.181E+15	.409E-06	.2216+03	1/0.08	0008+00	0.80	.437E+19	,433E+19	1576+16	343E+17	.2116-05	4.06+03	14.30	-1050-02
250.0	101E+17	.961E+16	,305E+15	.201E+15	.467E-06	.246E+03	176.30	.000E+00	\$6.0	.525E+19	,499E+19	.158E +18	.105E+18	.243E-05	.528E+05	73.05	.225E-02
245.0	.113E+17	.107E+17	.340E+15	.225E+15	.52IE-06	.274E+03	175.88	.000E+00	54.0	.599E+19	.569E+19	.180E+18	_120E+18	.2778-03	.595E+05	72.21	262E-00
240.0	.126E+17	.120E+17	.380E+15	.25IE+15	.582E-06	.305E+03	175.42	.000E+00	52.0	.682E+19	.648E+19	.205E+18	.136E+18	.315E-03	.673E+05	71.70	.30IE-02
235.0	141E+17	134E+17	.425E+15	.28IE+15	.650E-06	.340E+03	174.92	.000E+00	50.0	.775E+19	736E+19	232E+18	.155E+18	358E-03	.760E+05	71.35	:346E-02
2300	.158E+17	.150E+17	.475E+15	.314E+15	728E-06	.379E+03	174.39	.000E+00	48.0	.879E+19	.835E+19	.264E+18	.176E+18	.406E-03	.859E+05	71.11	395E-02
225.0	176E+17	.168E+17	_532E+15	.352E+15	815E-06	.423E+03	173.82	.000E+00	46.0	.998E+19	.948E+19	299E+18	.200E+18	461E-03	.972E+05	70.97	.451E-02
2200	198E+17	.188E+17	_596E+15	.394E+15	963E-06	4738+03	173.21	.000E+00	44.0	.10E+20	.108E+20	340E+18	.226E+18	52213-00	.100E+06	70.84	.513E-02
215.0	3330.1.17	2112 - 17	6690.14	4075.116	1020.05	\$300+03	173 69	00000+000	42.0	1200-20	1220 - 10	1860 - 19	257E-19	\$048.03	125E + 06	3164	587E-07
210.0	3405 - 15	0570 . 15	THE IS	A07E 136	HAT? DE	SOIE LOT	172.06	0000 : 00	42.0	1461 1 30	1300 1 20	4385 110	2075-10	6715 02	MIR-06	70.66	6660.00
2000	1900 - 17	2010111	RAAD OF	49712 113	1200.05	-3912 + 03	171.91	00000000	100	165121.00	15307-20	4040.110	1200-110	3612.00	1600 / 16	70.00	7445.02
2000	1+20/02	100E+1/	ATTE+D	-339E+13	1296-05	J02E+03	1/1.21	00000 000	560	1005+20	13/6+20	AP46716	33305-118		1000-100	21.10	9430.02
2000	368+17	.300E+17	.949E+15	AZ9E+15	10015-05	.7428.4-03	170.48	1000E 100	36.0	-186E   20	.1776120	359E118	.3738+18	3605-03	-18E+06	1.17	842B-02
198.0	.33IE+17	.314E+17	.996E+15	.660E+15	153E-05	.777E+03	170.18	.000E+00	34.0	.2HE+20	.200E+20	.632E+18	.421E+18	.972E-03	.205E+06	71,41	948E-02
196.0	_347E+17	.330E+17	.104E+16	.692E+15	.160E-05	B13E+03	169.88	.000E+00	32,0	.237E+20	.226E+20	.712E+18	.475E+18	.110E-02	.233E+06	71.81	.106E-01
									9/3.								
194.0	_364E+17	.346E+17	.10E+16	.726E+15	.168E-05	.852E+03	169.57	.000E+00	30.0	.267E+20	254E+20	801E+18	.534E+18	123E-00	.264E+06	72.34	.118E-01
192.0	.382E+17	.363E+17	.115E+16	.762E+15	.176E-05	392E+03	169.26	.000E+00	28.0	.300E+20	.285E+20	901E+18	.600E+18	_139E-02	.298E+06	72.92	.13IE-01
190.0	.400E+17	.38IE+17	.121E+16	.799E+15	185E-05	.934E+03	168.94	:000E+00	26.0	.336E+20	.319E+20	.101E+19	.673E+18	.155E-02	.337E+06	73.68	.145E-01
188.0	42/E+17	.400E+17	.127E+16	.839E+15	194E-05	979E+03	165.62	000E+00	24.0	.376E+20	.357E+20	.II3E+19	.752E+18	174E-02	.381E+06	74.55	.159E-01
184.0	4428-117	4206.117	133ELI6	SHELIS	204E-05	103E+04	158 30	0008+000	12.0	419E+20	398E+30	126E+19	\$37E+19	193E.m	429E+06	75.61	.173E-01
194.0	4640.117	4415-17	1404D-140	9350.115	21412-05	1075-04	165.07	0008+1000	200	467E-120	4446+30	140E+10	935E + 19	2161.02	484E 106	76.41	190E-01
182.0	4818.417	4638.497	MORA IN	OTELIS	2258.05	11384.04	167.64	0005+00	15.0	SIDE - 20	403E+30	1568.4.10	HOME + 10	2408.02	5458-06	27.60	206E.01
1020	.+0/E+1/	40/10 10/10	.P47E+10	.972B+15	2258-05	1000.004	107/04	MOD Pr	140	5000+20	546E 1 20	17206-119	TRACT IN	16.622 02	CINE - OF	70.04	2220 04
1800	512E+17	_480E+17	.D4E+10	.1021.+16	.2366-05	.1181-04	107.30	10005-04	16.0	.5/58/120	590G120	1726119	1000119	2036-02	.0110 106	16,55	4400 oc
178.0	.338E+17	.511E+17	.162E+16	.R07E+16	.248E-05	.124E+04	166.96	.100E-04	14.0	.6.55E+20	.604E+20	.191E+19	.12/E+19	293E-02	.68/E+06	80.19	239E-00
176.0	.565E+17	_537E+17	.IN0E+16	.113E+16	.261E-05	.130E+04	166.62	,100E-04	12.0	.70(E+20	.666E+20	210E+19	,140E+19	324E-02	.769E+06	81.56	.257E-01
									00410								600000
174.0	.594E+17	564E   17	.179E116	.118E   16	274E-05	.136E   04	166.27	,100E-04	10.0	.772E+20	.733E+20	.2325+19	.154E+19	.356E-02	.861E+06	83.00	.275E-01
172.0	.624E+17	_593E+17	.188E+16	.125E+16	.288E-05	.143E+04	165.92	.100E-04	80	.846E+20	.804E+20	.254E+19	.169E+19	.391E-02	.961E+06	\$4.72	.292E-01
1700	656E+17	623E+17	.197E+16	13IE+16	303E-05	150E+04	165.57	,100E-04	60	.925E+20	.879E+20	.278E+19	.185E+19	.427E-02	_107E+07	\$6,47	.309E-01
HIND	1590E-LT	ASSELT	2086416	ISKE 416	3946.05	1576+04	165 22	100E-04	50	.967E+20	9188+10	290E+12	191E+19	446E-02	.115E+07	\$7.40	317E-01
1660	776E + 17	600E 1 17	718E+16	LASE 116	1355 06	165E L 04	164 86	100E 04	40	10 E+21	960E+30	3037-10	2028+38	4678-02	199E+07	88 20	327E-04
161.0	764E-117	716E-117	2305+16	1528-16	3532.05	1738-104	164 50	NOE-04	30	105E+21	1008+21	316E+10	2112+19	486E.02	125E+07	89.26	335E-00
162.0	S042-17	364E (17	2425-16	MOP IN	1712 06	1925-04	164.14	1008 04	20	109E-121	104E+21	3285110	2105 + 10	505E-02	1326+07	90.54	330E.01
102.0	AVTE+IC	10+E+I/	1242E+10	100E+10	.5/IE-05	1625+04	104.14	1005-04	20	1150 - 02	30612 - 01	3360.419	2020 - 19	616D 00	1261 . 07	01.00	100.00
1600	340E+17	A048+17	234E+16	109E+16	390E-03	1918+04	103.77	1006-04	1.5	11213+21	100G+21	3356+19	122315+19	30-DC-02	.1000+07	71.60	0410-01
158.0	890E+17	,\$46E+17	.268E+16	.178E+16	.411E-05	.201E+04	163,41	_100E-04	10	.114E+21	.108E+21	34IE+19	_227E+19	.524E-02	139E+07	91.90	.343E-01
156.0	.938E+17	.891E+17	.232E+16	.187E+16	433E-05	211E+04	163.04	_100E-04	.5	.116E+21	.110E+21	.347E+19	.23IE+19	.534E-02	.143E+07	92.58	.345E-01
									1.500								
154.0	.987E+17	.938E+17	.297E+16	.197E+16	456E-05	222E+04	162.67	_100E-04	0	.118E+21	.112E+21	.353E119	.235E+19	.544E-02	.H6E+07	93.28	.347E-01
152.0	.104E+18	.988E+17	.3I3E+16	.208E+16	480E-05	.2335+04	162,29	.100E-04									
		A REAL PROPERTY AND	W12005701174	STATE OF STATE			10000										

Table 4. Minimum Yelle model for Titan's atmosphere. CH<sub>4</sub> 5% (larger in troposphere), Ar 0%, N<sub>2</sub> 95%, mean mass 27.40, T(1) = 175.0, T(2) = 135.0, T(3) = 175.0,  $\kappa = 0.100$ , A<sub>1</sub> = 0.044, A<sub>2</sub> = 0.006, A<sub>3</sub> = 0.000, Z<sub>h</sub> = 1100.0.

Z	Na	mber Der	r Densities (cm <sup>-3</sup> ) Mass Pressure Temp F Z Number Densities (cm <sup>-3</sup> )		Mass	Pressure	Temp	F									
(km)	Texal	N _2	CH	Ar	(gm/cm <sup>3</sup> )	(erg/cm <sup>3</sup> )	(K)		(km)	Total	N,	CH	Ar	(em/cm3)	(erg/cm))	(K)	
mania					10000	1000	36512					4	2.2				10221171
1206.0	2865+07	2448+07	.399E+00	.090E+00	.123E-15	.573E-07	145.00	.000E+00	8900	.137E+10	.130E+10	.705E+08	.000E+00	.622E-13	.273E-04	144.35	.000E+00
12950	326E+07	2816 +07	435E+06	000E+00	134E-15	A11E-07	145.00	000E+00	885.0	.149E+10	.142E+10	761E+08	.000E+00	.679E-13	.297E-04	144.14	.000E+00
1285.0	348E+07	300E+07	455E+06	000E+00	153E-15	675.07	145.00	000E+00	875.0	178E ± 10	.D3E+10 K0E+10	0/1E ± 08	000E+00	SOOE-13	353E-08	143.91	000E+00
1280.0	.372E+07	.325E+07	476E+06	.000E+00	164E-15	745E-07	145.00	000E+00	870.0	194E+10	184E+10	005E+08	000E+00	884E-13	385E-04	143.00	000E+00
1275.0	398E+07	348E+07	498E+06	.000E+00	ITSE-IS	.796E-07	145.00	.000E+00	865.0	.213E+10	.1040+10	104E+09	.000E+00	966E-13	420E-01	143.07	.000E+00
1270.0	.425E+07	373E+07	.521E+06	,000E+00	187E-15	.851E-07	145.00	.000E+00	850.0	.233E+10	.221E+10	.119E+09	.000E+00	.106E-12	458E-04	142.74	.000E+00
1265.0	.455E+07	,400E+07	.545E 1 06	.000E 100	_201E-15	.910E-07	145.00	00±3000.	855.0	.2550 ±10	.242E+10	.1342.+09	.000E+00	-11642-42	.500E-04	142.38	.000E+00
1260.0	.486E+07	.429E+07	.57IE+06	.000E+00	.215E-15	.973E-07	145.00	.000E+00	850.0	.279E+10	.265E+10	.142E+09	.000E+00	.127E-12	.547E-04	142.00	.000E+00
1255.0	_520E+07	,46) E+07	.599E+06	.000E+00	.230E-15	.104E-06	145.00	.000E+000	845.0	.306E+10	.290E+30	.155E+09	.000E±00	.139E-12	.598E-04	141.60	.000E+00
17500	5576407	4046 4 07	STILL OF	0000 + 00	2160.16	INP AS	116.00	0002-00	8600	1107 - 15	21027 ( 321	17017 - 00	0001-100	1030.10	17.15T 04	141.17	00000 - 000
12450	596E+07	\$34E+07	658E406	000E+00	240E-IS	10E-06	145/00	000E+00	8400	3355F+10 369E+10	.318E+10 350E+10	101E+09	000E+00	153E-12 167E-12	.004E-04	140.72	.000E+00
1240.0	638E+07	564E+07	590E+06	000E+00	283E-15	128E-06	145.00	(DOE+00	8300	405E+10	384E±10	205E+09	000E+00	184E-12	783E-04	140.75	000E+00
1235.0	.683E+07	.6UE+07	724E+06	000E+00	303E-15	137E-06	145.00	(00E+00	8250	445E+10	4228+10	225E+09	000E+00	2028-12	\$18E-04	13075	000E+10
1230.0	.732E+07	.656E+07	760E+06	.000E+00	.325E-45	.H6E-06	145.00	.000E+00	820.0	.489E+10	.465E+10	,248E+09	.000E+00	223E-12	.940E-04	139.23	.000E+30
1225.0	.784E+07	.704E+07	.798E+06	.000E+00	.349E-15	.157E-06	145.00	.000E+00	815.0	.539E+10	.512E+10	.272E+09	.000E+00	.245E-12	.103E-05	138.69	.000E+00
1220.0	.840E+07	.756E+07	.839E+06	.000E+00	.374E-15	.168E-06	145.00	.000E+00	810.0	.594E+10	.564E+10	.300E409	.000E+00	.2706-12	.1I3E-01	138.13	.000E+30
1215.0	.901E+07	.812E+07	.882E+06	,000E+00	.401E-15	.180E-06	145.00	.000E+00	805.0	.655E+10	.622E+10	.33IE+09	.000E+00	.298E-12	.124E-05	137.55	.000E+50
1230.0	.966E+07	.872E+07	.927E+06	.000E+00	.430E-I5	.193E-05	145.00	.000E+00	800.0	.723E+ID	.687E+10	.365E+09	.000E+00	.329E-12	.137E-03	136.94	.000E+00
1205.0	.1048+08	.934E+07	.975E+06	.000E+00	.462E-15	.207E-06	445.00	.000E+00	795.0	.799E+10	.259E+10	.403E+09	DODE+00	3638-12	.150E-03	136.32	.000E+30
12000	HIF-108	1012-105	10261-02	0002.100	3062.15	2225 06	11570	0005-000	7000		0302 10	A400 100		4025 12	HEFE OF	17000	DODE 130
105.0	100+08	1010-108	1092+07	0005 +00	,4905-15	-266E-00	145.00	00000000	7900	0795 + 10	.839E+10	.442E+09	00000 + 00	4028-12	.105E-05	132.08	.000E+30
190.0	.128E+08	_117E+08	1HE+07	000E+00	572E-15	256E-06	45.00	000E+00	783.0	108E+10	103E+10	\$46E+09	0008+00	4938-12	201E-03	134 34	000E+00
885.0	.137E+08	125E+08	.120E+07	.000E+00	.6HE-15	275E-06	145.00	(0)0E+00	775.0	120E+1	114E+11	605E+09	000E+00	547E-12	212E-08	13365	000E+30
180.0	147E+08	135E+08	127E+07	.000E+00	.660E-15	.205E-06	145.00	.000E+00	770.0	.133E+11	.127E+11	.67IE+09	.000E+C0	.607E-12	.245E-03	132.94	.000E+00
1175.0	.158E+08	.145E+08	.134E+07	.000E+00	.709E-15	.317E-06	145.00	.000E+00	765.0	.148E+11	.141E+11	.745E+09	.000E+00	.674E-12	.270E-03	132.21	.000E+30
1170.0	.170E+08	.156E+08	.141E+07	.000E+00	.762E-15	_340E-06	145.00	.000E+00	760.0	.165E+II	.157E+11	.829E+09	.000E+C0	.750E-12	.299E-03	131.46	.000E+30
165.0	.183E+08	.16EE+08	.149E+07	.000E+00	.820E-15	.366E-06	\$45.00	.000E+00	755.0	.184E+11	.1748+11	.922E+09	.000E+C0	.835E-12	:331E-03	130.70	.000E+30
160.0	.1968+08	.181E+08	.158E+07	,000E+00	.881E-15	.393E-06	145.00	.000E+00	750.0	.205E+11	.194E+11	.103E+10	.000E+00	.930E-12	.367E-03	129.93	.000E+00
455.0	.20E+08	.1948.+08	.167E+07	.000E+00	.948E-15	.422E-06	145.00	000E+00	745.0	,228E+II	.217E+11	.115E+10	D00E+00	104E-11	.407E-03	129.14	.000E+00
1150.0	2222 - 08	2010 + 00	17612 1 177	0005 + 00	1022-14	AT ATL OF	146.00	0000 :00	710.0	2555 - 11	2420114	12012 - 10	0000 - 00	1167 11	1000 00	120.24	00000 1000
8450	244F+08	225E+08	1875+07	000E+00	102E-14	434E-06	145.00	000E+00	7400	285E+11	2428+11	141E+10	0008+00	130E-11	-452E-08	128.34	000E+00
840.0	.263E+08	.243E+08	198E+07	.000E+00	10E-14	325E-06	145.00	000E+00	7300	.2836+11 .319E+11	.2/1E+11	160E+10	DODE+00	145E-11	518E-03	1267	.000E+00
135.0	283E+08	262E+08	209E+07	.000E+00	127E-14	565E-06	145.00	000E+00	7250	358E+11	340E+11	179E+10	000E+00	163E-11	671E-07	12588	.000E+00
1130.0	304E+08	.282E+08	.222E+07	.000E+00	137E-14	.608E-06	145.00	.000E+00	720.0	.401E+11	.38IE+11	.201E+10	000E+00	183E-11	.693E-03	125.04	,000E+00
125.0	.327E+08	.304E+08	.235E + 07	.000E+00	.147E-H	.655E-06	145.00	.000E+00	715.0	.451E+11	.428E+II	.226E+10	.000E+00	205E 11	.773E 03	\$24.20	.000E+00
120.0	-352E+08	.327E+08	.250E+07	.000E+00	.159E-14	.705E-06	145.00	.000E+00	710.0	.507E+11	.482E+11	.254E+10	000E+00	.231E-11	.863E-03	123.35	.000E+00
1115.0	.380E+08	.353E+08	.265E+07	.000E+00	.171E-14	.760E-06	145.00	.000E+00	705.0	.571E+11	.542E+11	.286E+10	000E+00	260E-11	.965E-03	122.49	.000E+00
1110.0	.409E+08	.381E+06	.282E+07	.000E+00	.184E-14	.818E-06	145.00	.000E+00	700.0	.644E+II	/611E+11	.323E+10	000E+00	293E-11	,108E-01	121.63	.000E+00
105.0	.441E+08	.41E+08	.300E+07	T000E+00	.199E-14	.882E-06	145.00	.000E+00	695.0	.727E+1	.690E+11	.364E+10	000E+09	330E-11	.124E-02	120.77	.000E+00
1000	4752	4478+08	3105-1-07	0006 ± 00	DIAE M	0500.05	145.00	0005100	600.0	971E 1.11	19001-111	4007.1.00	00081.00	2220.01	1261 (0)	110.01	0000 - 000
1005.0	512E +08	478E+08	3400+07	000E+00	2115.14	1930E-06	145.00	0005+00	6850	0206-11	-18065+11 9920-11	4652 + 10	000E+00	4235-11	1532.01	119.91	00000+00
1090.0	.552E+08	_516E+08	.362E+07	.000E+00	249E-14	.10E-05	145.00	.000E+00	680.0	105E+12	.100E+12	.527E+10	000E+00	479E-II	.172E-02	118.19	.000E+00
1085.0	595E+08	557E+08	.386E+07	.000E+00	_269E-14	.119E-05	145.00	.000E+00	675.0	.119E+12	.113E+12	.598E+10	000E+00	5438-11	.153E-02	117.34	.000E+00
1080.0	.642E+08	60IE+08	.4IIE+07	.000E+00	.290E-14	.128E-05	145.00	.000E+00	670.0	.136E+12	.129E+12	.679E+10	.000E+00	.617E-II	.218E-03	116.49	.000E+00
1075.0	.693E+08	.649E+08	.439E+07	4000E 1 00	.3I3E-14	.139E-05	145.00	.000E 100	665.0	.154E+12	.146E+12	.771E+10	00+3000	.701E-11	.246E-02	115.66	.000E+00
1070.0	748E+08	.701E+08	.469E+07	.000E+00	.338E-14	.150E-05	145.00	.000E+00	660.0	.175E+12	.167E+12	.879E+10	000E+00	.798E-11	.278E-02	114.83	.000E+00
1065.0	.807E+08	.757E+08	_501E+07	.000E+00	.365E-14	.162E-05	145.00	.000E+00	655.0	.200E+12	.1905+12	.100E+II	000E+00	.910E-II	.315E-02	114.02	.000E+00
1050.0	372E+08	SISE+08	-555E+07	000E+00	.394E-14	.1/4E-05	145.00	000E+00	6300	.ZZ8E+12	.217E+12 248E+12	.114E+11 13007+18	000E+00	.304E-10	.357E-00	113.22	.000E+00
103330	,9410-100	2001E-FV0	.5726+07	.0001100	.420E-14	.1995-00	145000	10012-100	04300	.2015 +12	-2486712	1396.11	DODETON	.096-00	,4008-01	112.45	1006+00
1050.0	.102E+09	956E+08	6I3E+07	000E+00	460E-14	203E-05	145.00	000E+00	640.0	298E+12	2838+12	1448-11	000E+00	136E-10	460E-02	111.69	000E+00
1045.0	.II0E+09	.103E+09	656E+07	.000E+00	.498E-14	.220E-05	145.00	.000E+00	635.0	.34IE+12	.324E+12	.17IE+11	.000E+00	155E-10	.523E-02	110.96	.000E+00
1040.0	.119E+09	.II2E+09	.703E+07	.000E+00	.538E-14	.238E-05	145.00	.000E+00	630.0	,391E+12	.372E+12	.196E+11	.000E+00	.178E-10	.595E-02	110.25	.000E+00
1035.0	.128E+09	.121E+09	.753E+07	.000E+00	.582E-14	.257E-05	145.00	.000E+00	625.0	.449E+12	.427E+12	,225E+II	.000E+00	204E-10	.679E-01	109.58	.000E+00
1030.0	.139E+09	.13IE+09	808E+07	.000E+00	.629E-14	.278E-05	145.00	.000E+00	620.0	.516E+12	.490E+12	.258E+11	.00+3000	235E-10	.775E-01	108.93	.000E+00
1025.0	.150E+09	.14IE+09	.867E+07	.000E+00	.6808-14	.300E-05	145.00	.000E+000.	605.0	.593E+12	.3636+82	.2968.+11	00+300	270E-10	.886E-03	108.33	.000E+00
1020.0	.162E+09	.153E+09	931E+07	.000E+00	.736E-14	.325E-05	145.00	.000E+00	610.0	.682E+12	.648E+12	.34/E+II	.000E+00	.310E-10	_101E-01	107.76	.000E+00
1015.0	1205+09	17002+09	100E+08	300E+00	./9/E-04	.352E405	145.00	D00E+00	600.0	.7856+12	./405+12	.3938.+0	000E+00	357E-10	.108-01	107.23	D00E+00
1005.0	.206E+09	.194E+09	.106E+08	.000E+00	934E-14	428.05	145.00	.000E+00	5050	.304E+12	.839C+12 .990E+12	571EAU	000E+00	4748.30	1536-01	106.33	.000E+00
and and		10/10/102		Second Land	130.17.14	Chep.00	115100	3705100	0100	1000210	13700112	1740678	JUNDITO	111210	1000-01	100.00	5005700
1000.0	.2238+09	.210E+09	.124E+08	.000E+00	.101E-13	.446E-05	145.00	.000E+00	590.0	.120E+13	.84E+13	.60(E+1)	.000E+00	.546E-10	.1%E-01	105.95	.000E+00
995.0	.241E+09	228E+09	134E+08	.000E+00	.110E-13	.483E-05	145.00	.000E+00	585.0	.139E+13	.132E+13	693E+11	.00)E+0)	630E-10	.202E-0	105.63	000E+00
990.0	.261E+09	.247E+09	.144E+08	.000E+00	.119E-13	.523E-05	145.00	.000E+00	580.0	.160E+13	.152E+13	.800E+II	.000E+00	727E-10	.233E-01	105.38	.000E+00
985.0	.283E+09	.268E+09	.156E+08	_000E+00	.129E 13	.567E 05	145.00	.000E+00	\$75.0	.185E+13	.175E+13	.923E+II	,000E 1 00	839E-10	.268E-0	105.18	.000E + 00
980.0	.307E+09	_290E+09	.168E+08	.000E+00	.139E-13	.04E-05	145.00	.000E+00	570.0	213E+13	.202E+13	.107E+12	.000E+00	969E-10	.309E-0)	105.06	.000E+00
975.0	.333E+09	.315E+09	.18IE+06	.000E+00	.151E-13	.656E-05	145.00	.000E+00	565.0	.246E+13	.233E+13	.123E+12	.000E+00	112E-09	.356E-01	105.00	.000E+00
9/0.0	.301E+09	.34E+09	.195E+08	000E+00	.164E-13	.722E-05	145.00	.090E+00	560.0	.283E+13	.269E+13	.142E+12	1000E+00	129E-09	.4.IE-01	105.03	.000E+00
900.0	.391E+09	A00E 108	119E+08	000E+00	.178E-13	-783E-05	145.00	.000E+00	555.0	327E+13	3105.413	163E+12	0008+00	149E-09	.434E-0)	105.17	000E+00
955.0	.461E+09	436E+09	246F+08	D00E+00	.209E-13	.922E.05	145.00	.000E+00	5450		4115+13	217E+12	000E+00	197E-09	6325-0	105.42	000E+00
					100000-10	17.884.762	a fundina		01000	CTOOL T D		ALCO THE	20000-000	17/12/09	NUMBER OF	10033	
950.0	.500E+09	.473E+09	.266E+08	.000E+00	.227E-13	.100E-04	145.00	.000E+00	540.0	.498E+13	.473E+13	.249E+12	.000E+00	226E-09	.730E-01	106.21	.000E+00
945.0	.543E+09	.514E+09	.288E+08	000E+00	.247E-13	109E-04	145.00	000E+00	535.0	572E+13	.543E+13	286E+12	.000E+00	260E-09	.842E-01	106.75	.000E+00
940.0	.5898+09	.558E+09	.3IIE+08	.000E+00	.268E-13	.18E-04	145.00	.000E+00	530.0	.656E+13	.623E+13	.321E+12	.000E+00	.298E-09	.972E-01	107.37	.000E+00
935.0	640E+09	.606E+09	.337E+08	.000E+00	.291E 13	.128E 04	145.00	.000E+00	525.0	.752E+13	.714E 13	.376E+12	.000E 1 00	.342E-09	.112E   00	108.07	.000E+00
930.0	.695E+09	655E+09	_365E+08	.000E+00	.3)6E-I3	.139E-04	145.00	.000E+00	520.0	.860E+13	.8J7E+13	.430E+12	.000E+00	.391E-09	129E+00	108.84	.000E+00
925.0	-/36E+09	7766+09	-396E+08	000E+00	.343E-13	.DIE-04	145.00	.010E+00	515,0	.984E+13	.934E+13	.492E+12	.000E+00	.447E-09	.149E+00	109.69	.000E+00
92000	8036-00	A3E+09	42912+08	000E+00	-3/3E-13 406E-13	104E-04	144.99	.000E+00	510.0	1122+14	.107E+14	_302E+12	000E+00	501E-09	.171E+00	110.60	.000E+00
100	972E+09	921E+06	305E+08	00+3000	44212-13	1941-04	144.93	000E+00	5000	146E+14	199E+14	730E+12	0008+00	564E-09	2278+00	112.56	000E+00
905.0	-106E+10	100E+10	548E+08	.000E+00	.481E-13	211E-04	144.79	.010E+00	495.0	.166E+14	.158E+14	\$30E+D	.000E+00	755E-09	260E+00	113.64	.000E+00
19.00								C.C.C.C.C.C.							3000.100		
900.0	.II5E+10	.105E+10	.595E+08	.06015-000	.524E-13	.230E-04	144.67	.010E+00	490.0	.189E+14	.179E+14	.944E+12	.000E+00	358E-09	_299E+00	114.75	.000E+00
895.0	-1268+10	.119E+10	.648E+08	.000E+00	.57IE-13	_250E-04	144.52	.000E+00			-			1000	con	ntinued or	next page

Table 4. (Continued).

A. Dame         Description (100)         Allis         Prissip         Description (100)         Description (100)         Description (100)         Prissip         Description (100)           Bill         Mail         C. C.         C. C.         Allis         Number (100)         Number (100) <t< th=""><th>2</th><th>N.</th><th>the Day</th><th>and the second</th><th>-3,</th><th>Maria</th><th>Deserves</th><th></th><th>F</th><th></th><th colspan="2">7 Note Deside (3)</th><th></th><th></th><th></th><th></th></t<>	2	N.	the Day	and the second	-3,	Maria	Deserves		F		7 Note Deside (3)							
Name         Name <th< th=""><th>(km)</th><th>Total</th><th>N<sub>2</sub></th><th>CH<sub>4</sub></th><th>Ar</th><th><math>(gm/cm^3)</math></th><th>(erg/cm<sup>3</sup>)</th><th>(K)</th><th>r,</th><th>Z (km)</th><th>Nı Total</th><th>unber Dei N<sub>2</sub></th><th>uities (cm CH<sub>4</sub></th><th>Ar</th><th>Mass (gm/cm<sup>3</sup>)</th><th>Pressure (erg/cm<sup>3</sup>)</th><th>Temp (K)</th><th>F.</th></th<>	(km)	Total	N <sub>2</sub>	CH <sub>4</sub>	Ar	$(gm/cm^3)$	(erg/cm <sup>3</sup> )	(K)	r,	Z (km)	Nı Total	unber Dei N <sub>2</sub>	uities (cm CH <sub>4</sub>	Ar	Mass (gm/cm <sup>3</sup> )	Pressure (erg/cm <sup>3</sup> )	Temp (K)	F.
min         min <td>485.0</td> <td>714E+14</td> <td>2045-14</td> <td>107E+13</td> <td>000E±00</td> <td>075E.00</td> <td>3436100</td> <td>115 80</td> <td>000E-00</td> <td>150.0</td> <td>718E±17</td> <td>687E±17</td> <td>3405+16</td> <td>000E+00</td> <td>326E-05</td> <td>1448+04</td> <td>145.77</td> <td>1008-04</td>	485.0	714E+14	2045-14	107E+13	000E±00	075E.00	3436100	115 80	000E-00	150.0	718E±17	687E±17	3405+16	000E+00	326E-05	1448+04	145.77	1008-04
10.         10. <td>480.0</td> <td>243E+14</td> <td>23E+M</td> <td>122E+13</td> <td>.000E+00</td> <td>.10E-08</td> <td>.393E+00</td> <td>117.06</td> <td>.000E-00</td> <td>148.0</td> <td>.760E+17</td> <td>722E+17</td> <td>380E+16</td> <td>.000E+00</td> <td>.346E-05</td> <td>152E+04</td> <td>144 92</td> <td>100E-04</td>	480.0	243E+14	23E+M	122E+13	.000E+00	.10E-08	.393E+00	117.06	.000E-00	148.0	.760E+17	722E+17	380E+16	.000E+00	.346E-05	152E+04	144 92	100E-04
Dia         Dia <thdia< th=""> <thdia< th=""> <thdia< th=""></thdia<></thdia<></thdia<>	475.0	.275E+14	.262E+14	.138E+13	,000E+00	.125E-08	,449E+00	118.26	.000E-00	146.0	.830E+17	.759E+17	.405E+16	.000E+00	.368E-05	.161E+04	143.76	.100E-04
mod         mod <td>47010</td> <td>.312E+14</td> <td>.296E+14</td> <td>.156E+13</td> <td>.000E+00</td> <td>.142E-08</td> <td>.5i4E+00</td> <td>119,48</td> <td>.000E-00</td> <td>144.0</td> <td>.853E+1?</td> <td>.810E+17</td> <td>.426E+16</td> <td>.000E+00</td> <td>.388E-05</td> <td>.170E+04</td> <td>144.37</td> <td>.100E-04</td>	47010	.312E+14	.296E+14	.156E+13	.000E+00	.142E-08	.5i4E+00	119,48	.000E-00	144.0	.853E+1?	.810E+17	.426E+16	.000E+00	.388E-05	.170E+04	144.37	.100E-04
1000         1000 <th< td=""><td>405.0</td><td>357E+14 309E+14</td><td>3332+14</td><td>176E+13 100E+13</td><td>000E+00</td><td>191E-08</td><td>.587E+00 670E+00</td><td>120.71</td><td>.000E-00</td><td>142.0</td><td>.9RE+17 067E+17</td><td>.854E+17 00E±17</td><td>453E+16</td><td>000E+00</td><td>440E-05</td><td>180E+04 190E+04</td><td>147 31</td><td>100E-04</td></th<>	405.0	357E+14 309E+14	3332+14	176E+13 100E+13	000E+00	191E-08	.587E+00 670E+00	120.71	.000E-00	142.0	.9RE+17 067E+17	.854E+17 00E±17	453E+16	000E+00	440E-05	180E+04 190E+04	147 31	100E-04
ety         y 114         y	455.0	.449E+14	.42'E+14	.225E+13	.000E+00	.204E-08	.764E+00	123.21	.000E-00	138.0	.102E+18	.574E+17	512E+16	000E+00	.466E-05	201E+04	142.11	.100E-04
401         7.01         3.01         3.00000         1000        1000        1000	450.0	507E+14	.48E+M	.253E+13	.000E+00	.230E-08	.870E+00	124.47	.000E-00	136.0	.109E+18	.104E+18	545E+16	.000E+00	.496E-05	213E+04	141.41	.100E-04
	445.0	.571E+14	.542E+14	.285E+13	.000E+00	.260E-08	.990E+00	125.73	.000E-00	134.0	.116E+18	.BOE-18	.578E+16	.000E+00	.526E-05	225E+04	141.24	.200E-04
10.10         2014 <t< td=""><td>440.0</td><td>.643E+14</td><td>.611E+14</td><td>3216+13</td><td>.000E+00</td><td>.292E-08</td><td>.IBE+00</td><td>126.98</td><td>.000E-00</td><td>132.0</td><td>.123E+I#</td><td>.117E-18</td><td>.614E+16</td><td>.000E+00</td><td>.559E-05</td><td>2398+04</td><td>140.58</td><td>.200E-04</td></t<>	440.0	.643E+14	.611E+14	3216+13	.000E+00	.292E-08	.IBE+00	126.98	.000E-00	132.0	.123E+I#	.117E-18	.614E+16	.000E+00	.559E-05	2398+04	140.58	.200E-04
100              101              001              001              001              001              001              001              001              001              001              001              001              001              001              001001             00101            00101111	435.0	.723E+14	.687E+14	.362E+13	.000E+00	.329E-08	.128E+01	128.23	.000E-00	130.0	.130E+18	.124E+18	.65IE+16	.000E+00	.592E-05	253E+04	140.63	.200E-04
100         1010         10111         1011         1011 <th< td=""><td>430.0</td><td>.813E+14</td><td>.773E+14</td><td>.407E+13</td><td>.000E+06</td><td>.370E-08</td><td>.145E+01</td><td>129.46</td><td>.000E-00</td><td>128.0</td><td>.139E+18</td><td>.B2E+18</td><td>.695E+16</td><td>000E+00</td><td>A32E-05</td><td>268E+04</td><td>139.52</td><td>.200E-04</td></th<>	430.0	.813E+14	.773E+14	.407E+13	.000E+06	.370E-08	.145E+01	129.46	.000E-00	128.0	.139E+18	.B2E+18	.695E+16	000E+00	A32E-05	268E+04	139.52	.200E-04
IIII IIII IIIII IIIIIIIIIIIIIIIIIIIII	420.0	103E+15	.975E+14	513E+13	000E+00	467E-08	107E+01	131.88	.000E-00	124.0	.149E+18	.150E+18	79/E+16	000E+00	320E-05	301E+04	137.77	.200E-04
	415.0	.115E+15	.100E+15	.576E+13	.000E+00	.524E-08	.212E+01	133.06	.000E-00	122.0	.169E+18	.161E-18	.847E+16	.000E+00	.771E-05	319E+04	136.53	.200E-04
0000         00000         000000         00000000         000000000000000000000000000000000000	410.0	.129E+15	.123E+15	/647E+13	.000E+00	.589E-08	.240E-01	134.21	.000E-00	120.0	.181E+18	.172E+18	.903E+)6	.000E+00	.822E-05	.339E+04	135.03	.300E-04
<ul> <li>Martin Martin Marti Martin Martin Martin Martin Martin Martin Martin Martin Mart</li></ul>	405.0	.145E+15	138E+15	J26E+13	.000E+00	.660E-08	.271E+01	135.34	.000E-00	1180	.193E+18	.B3E+18	.964E+16	.000E+00	.877E-05	360E+04	135.35	.300E-04
9960              2014-19              0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00             0014-00	400.0	1036+15	171E+15	814E+13	000E+00	.741E-08	_307E+01	136.43	.000E-00	116.0	206E+18 210E+18	195E+18 199E+19	100E+17	J000E+00	.935E-05 007E-05	382E+04	134.82	.300E-04
1000         2001-10         2001-10         2001-10         2002-10         2001-10         2	390.0	.205E+15	.194E+15	J02E+14	.000E+00	.931E-08	.391E+01	138.52	.000E-00	112.0	.234E+18	.223E+18	.10E+17	.000E+00	.107E-04	.432E+04	133.57	.300E-04
1000              2017-13              2017-14              2017-14              2017-14              2017-14              2017-14              2017-14              2017-14              2017-14              2017-14              2017-14              2017-14              2017-14	385.0	.229E+15	.218E+15	.IISE+14	.000E+00	.104E-07	442E-01	139.50	.000E-00	1100	250E+18	.238E+18	.125E+17	000E+00	114E-04	459E+04	132.97	.401E-04
355         356         3564         3664         3564         3	380.0	.257E+15	.244E+15	.129E+14	.000E+00	.117E-07	.498E-01	140.44	.000E-00	108.0	.267E+18	.254E+18	.134E+17	.000E+00	.122E-04	489E+04	132.55	.401E-04
100         2016         3016-5         3016-6         3016-6         3016-7	375.0	.288E+15	.274E+15	.144E+14	.000E+00	.131E-07	.562E-01	141.34	.000E-00	106.0	.286E+18	.271E+18	.143E+17	.000E+00	.130E-04	.520E+04	131.96	.401E-04
No.         Active 3         Bite 14         Dolle 14 <thdolle 14<="" th=""> <thdolle 14<="" th=""> <thdole< td=""><td>370.0</td><td>.323E+15</td><td>.307E+15</td><td>.162E+14</td><td>.000E+00</td><td>.147E-07</td><td>.634E+01</td><td>142.19</td><td>.000E-00</td><td>104.0</td><td>.307E+18</td><td>.292E+18</td><td>_154E+17</td><td>.000E+00</td><td>.140E-04</td><td>.554E+01</td><td>130.52</td><td>.499E-04</td></thdole<></thdolle></thdolle>	370.0	.323E+15	.307E+15	.162E+14	.000E+00	.147E-07	.634E+01	142.19	.000E-00	104.0	.307E+18	.292E+18	_154E+17	.000E+00	.140E-04	.554E+01	130.52	.499E-04
1553         4664-14         4018-15         3281-14         20081-00         2276-07         20081-00         2276-07         20081-00         2276-07         20081-00         2276-07         20081-00         2276-07         20081-00         20081-0	365.0	.362E+15	394E+15	181E+14 NOTE+14	.000E+00	.165E-07	.715E+00	142.98	.000E-00	102.0	.330E+18	.313E+18 117E+19	_165E+17	000E+00	150E-04 161E-04	.590E+04 620E+04	129,58	.499E-04
1000         STE-15         STE-15         STE-14         STE-15         STE-16         STE-15         STE-16         STE-15         STE-16         STE-15         STE-16         STE-16 <td>355.0</td> <td>400E+13</td> <td>_309E+15</td> <td>.205E+14</td> <td>.000E+00</td> <td>2078-07</td> <td>200E+01</td> <td>144.41</td> <td>.000E-00</td> <td>080</td> <td>.333E+18</td> <td>.357E+18</td> <td>10/E+17</td> <td>000E+00</td> <td>101E-04</td> <td>671E+04</td> <td>127.58</td> <td>600E-04</td>	355.0	400E+13	_309E+15	.205E+14	.000E+00	2078-07	200E+01	144.41	.000E-00	080	.333E+18	.357E+18	10/E+17	000E+00	101E-04	671E+04	127.58	600E-04
945         9521         53221:15         5322:14         5322:14         5322:14         5322:14         5322:14         5322:14         5322:14         5322:14         5322:14         5322:14         5322:14         5324	350.0	.511E+15	.485E+15	.255E+14	.000E+00	.232E-07	.02E+02	145.06	.000E-00	960	.410E+18	.390E+18	205E+17	.000E+00	.187E-04	.716E+04	126.55	.700E-04
466              506             506            5	345.0	.572E+15	_543E+15	.286E+14	.000E+00	.260E-07	.115E+02	145.95	.000E+00	94.0	.443E+18	.421E+18	_222E+17	.000E+00	.202E-04	765E+04	125.09	.700E-04
31.93         31.93         31.95         375.12         30.95.07         30.95.	340.0	.641E+15	.609E+15	.320E+14	.000E+00	.291E-07	.130E+02	146.77	00-E000	92.0	.480E+18	,456E+18	.2408+17	.000E+00	,219E-04	_\$18E+04	123.39	.800E-04
306         306         3064:1-3         5064:1-4         3002:	335.0	.717E+15	.682E+15	.359E+14	.000E+00	.326E-07	.146E+02	147.53	.000E-00	90.0	.519E+18	.493E+18	.259E+17	.000E+00	.236E-04	.875E+04	122.34	.900E-04
133         133         134         500: 1	330.0	.804E+15	.764E+15	.402E+14	.000E+00	.366E-07	.164E+02	148.24	.000E-00	880	_558E+18	.530E+18	.279E+17	000E+00	.254E-04	.937E+04	121.83	.100E-03
1500         1510-8 <td>325.0</td> <td>301E+15</td> <td>859E+15</td> <td>.450E+14</td> <td>000E+00</td> <td>.410E-07</td> <td>.INSE+02</td> <td>148.88</td> <td>.000E-00</td> <td>86.0</td> <td>.506E+18</td> <td>.576E+18</td> <td>.303E+17</td> <td>000E+00</td> <td>276E-04</td> <td>100E+05</td> <td>120.02</td> <td>120E-03</td>	325.0	301E+15	859E+15	.450E+14	000E+00	.410E-07	.INSE+02	148.88	.000E-00	86.0	.506E+18	.576E+18	.303E+17	000E+00	276E-04	100E+05	120.02	120E-03
100         202+16         122+14         000+00         535:07         244:0         000-0         500         3000-100	315.0	.II3E+16	.108E+16	.505E+14	.000E+00	.409E-07	.206E+02	150.02	.000E-00	82.0	.732E ( 18	.605E+18	.352E+17	.000E+00	.333E-04	.116E+05	114.71	.140E-03
365         132±+6         132±+6         132±+6         132±+6         102±+6         102±+6         102±-6 <td>310.0</td> <td>.127E+16</td> <td>.12IE+16</td> <td>.635E+14</td> <td>.000E+00</td> <td>.578E-07</td> <td>.264E+02</td> <td>150.50</td> <td>.000E-00</td> <td>800</td> <td>.806E+18</td> <td>.766E+18</td> <td>.403E+17</td> <td>000E+00</td> <td>.367E-04</td> <td>125E+05</td> <td>112.14</td> <td>.160E-03</td>	310.0	.127E+16	.12IE+16	.635E+14	.000E+00	.578E-07	.264E+02	150.50	.000E-00	800	.806E+18	.766E+18	.403E+17	000E+00	.367E-04	125E+05	112.14	.160E-03
1000         2000t+00         152t+16         2000t+10         252t+16         2000t+10         252t+16         2000t+10         20	305.0	.142E+16	.135E+16	.712E+14	.000E+00	.648E-07	.297E+02	150,94	.000E+00	780	.893E+18	.848E+18	.447E+17	.000E+00	.406E-04	135E+05	109.20	.190E-03
2010         302+16         JUL-16         JUL-10         JUL-10 <thjul-10< td="" th<=""><td>300.0</td><td>.160E+16</td><td>152E+16</td><td>.800E+14</td><td>.000E+00</td><td>.728E-07</td><td>.334E ( 02</td><td>151.33</td><td>.000E 00</td><td>760</td><td>.990E+18</td><td>.940E+18</td><td>.495E+17</td><td>.000E+00</td><td>.450E-04</td><td>145E+05</td><td>106.54</td><td>.220E 03</td></thjul-10<>	300.0	.160E+16	152E+16	.800E+14	.000E+00	.728E-07	.334E ( 02	151.33	.000E 00	760	.990E+18	.940E+18	.495E+17	.000E+00	.450E-04	145E+05	106.54	.220E 03
255       272F+16       206E+16       313E+15       000E+00       105E+06       377E+10       212.9       000E+00       105E+19       377E+10       202E+17       000E+00       557E+04       187E+05       93.86       400E-30         2800       253E+16       242E+16       00E+10       11E+66       537E+10       122.4       000E+00       1661       900E+19       900E+19       900E+19       10E+19       10E+1	295.0	.180E+16 .202E+16	.17(E+16	.898E+14 .001E+15	.000E+00	.908E-07	.3%E+02 .423E+02	151.67	.000E-00	74.0	.110E+19 .125E+19	.105E+19 .119E-19	.550E+17 .624E+17	.000E+00	.500E-04 .568E-04	.158E+05 .171E+05	99.50	.250E-03
$ \begin{array}{c} 200 & 221+16 & 206+76 & 312+15 & 300+10 & 302+0 & 472+70 & 32.9 & 900+70 & 302+76 & 322+60 & 302+60 & 3$	1050	2025-16	DIST: N		00000 - 000	10370.046	4535.02		00010 00	-		10700 - 100		000E - 00	CETE 04	1070 . 05	01.64	1000 00
2556       257E 1.6       277E 1.6       107E 46       200E 1.9       200E	2850	255E+16	241E+16	108E+15	000E+00	USE-06	.4:7E+02 537E+02	152.19	000E-00	680	168E+19	150E+19	339E±17	000E+00	.057E-04	205E+05	93.60	\$10E-03
Tub         3248-16         307E+16         30	275.0	.287E+16	.273E+16	.144E+15	.000E+00	.131E-06	.605E+02	152.54	.000E-00	660	.200E+19	.190E+19	_100E+18	.000E+00	.9128-04	227E+05	82.01	.700E-03
3656         3658-16         3478-16         3488-16         5678-188-10         3488-16         5678-188-10         3488-16         5678-188-10         3478-16	270.0	,324E+16	.307E+16	.162E+15	.000E+00	.147E-06	.682E+02	152.66	.000E+00	64.0	.242E+19	.230E+19	.12:E+18	.000E+00	.100E-03	.252E+05	75,74	.970E-03
2000         AllE 16         3961-16         2001-40         JBF146         3971-402         192.75         JODE-10         500         3951-44         JODE-10         3001-00         1841-43         33208-103         6675         JBE40           2500         JSE14-15         JODE-10         JSE14-03         JSE14-15         JODE-10         JSE14-15         JSE14-15<	265.0	.365E+16	_347E+16	.182E+15	.000E+00	.166E-06	.769E+02	152.72	.000E-00	62.0	.288E+19	.274E+19	.144E+18	.000E+00	13IE-03	283E+05	71.31	.128E-02
1233       4341=16       441+15       1241+15       0001+00       2024-03       0002+00       2024-03       0002+00       2024-03       441±+03       2024-03       441±+03       2024-03       441±+03       2024+03       441±+03       2024+03       441±+03       2024+03       441±+03       2244       6501±+03       2024-03       441±+03       2244±+03       6514±       331±+03       944±+18       0001±+00       231±+03       441±+03       524±+03       451±+03       231±+03       441±+03       524±+03       451±+03       524±+03       451±+03       531±+03       <	260.0	,411E+16	_39/E+16	.206E+15	.000E+00	.187E-06	.867E+02	152.75	.000E-00	600	.336E+19	.322E+19	.169E+18	.000E+00	.154E-03	.320E 1 05	68,67	.16IE-02
2450       992E+16       563E+6       952E+16       500E+06       299E-63       47E+05       662E+0       325E+03       122.55       000E+00       526E+19       490E+19       240E+18       000E+00       27E+03       538E+05       6508       31E+05       012.95         2536       758E+16       53EE+15       000E+00       .345E+66       .94E+03       122.0       000E+00       122.0       .000E+00       .342E+63       000E+03       .53EE+03       012.66       .000E+00       .342E+64       .000E+04       .342E+03       064E+03       .53EE+03       .000E+04       .53EE+03	250.0	464E+16 574E+16	.44.E+16	252E+15	000E+00	_218E-06	.9/8E+02	152.74	000E-00	580	_395E+19 _458E+19	435E+19	2208 + 18	000E+00	180E-03 208E-03	303E+05 414E+05	65.64	236E-02
2400       670E+16       638E+6       335E+15       000E+00       355E+05       199E+03       152.0       600E+19       571E+19       330E+18       000E+00       332E+03       6546       352E+02         2350       798E+16       78E+16       78E+16       78E+16       37E+03       332E+03       654E+03       650E       366E+04       651E+0       332E+03       335E+03       664E+03       650E       366E+04       651E+0       352E+03       336E+03       656E       366E+04       651E+0       352E+03       306E+04       651E+0       352E+03       306E+04       651E+0       352E+03       306E+04       651E+0       352E+03       306E+04       651E+0       552E+03       306E+04       651E+0       552E+03       106E+04       651E+0       552E+03       106E+04       651E+0       552E+03       106E+06       651F       552E+03       106E+06       651F       552E+03       106E+06       651F       552E+03       105E+06       654E       746E+05       306E+06       552E+03       105E+06       654E       746E+03       552E+03       155E+06       654E       746E+03       552E+03       155E+06       654E       746E+03       552E+03       155E+06       654E       746E+03       552E+03       155E+06<	245.0	.592E+16	_563E+16	.296E+15	.000E+00	.269E-06	.125E+03	152.59	.000E-00	54.0	.526E+19	.499E+19	.263E+18	J000E+00	.239E-03	471E+05	65.19	.274E-02
3350       758E+86	240.0	.670E+16	.636E+)6	.335E+15	.000E+00	.305E-06	.141E+03	152.46	.000E00	52.0	.601E+19	.571E+19	.30IE+18	.000E+00	.273E-03	.538E+05	65.06	.315E-02
2100         859E+16         512E+10         300E+00         355E+03         700E+05         65.47         462E-02           2206         978E+16         902E+17         552E+16         302E+103         151.7         000E+104         352E+10         355E+10         355E+10         355E+10         355E+10         355E+10         355E+10         355E+10         355E+10	235.0	.758E+16	.720E+16	.379E+15	.000E+00	.345E-06	.159E+03	152.30	.000E-00	50.0	.686E+19	.652E+19	.343E+18	.000E+00	.312E-03	.614E+05	65.09	.360E-02
1213       0.94/E+16       0.94/E+16       0.01E+10       0.00E+10       0.01E+10       0	230.0	.859E+16	.816E+16	.429E+15	.000E+00	.391E-06	.190E+03	152.10	.000E+00	48.0	.782E+19	.742E+19	_391E+18	.000E+00	.355E-03	.701E+05	65.26	.408E-02
2150       0.25E+17       118E+17       212E+18       000E+00       57E=64       502E+03       151.30       000E+00       420       115E+20       57E=+8       000E+00       524E-03       104E+06       65.37       522E-03       152E+17       102E+17       128E+17       128E+17       128E+15       000E+00       354E-03       100E+06       557E+8       000E+00       354E-03       100E+06       65.37       557E+8       000E+00       354E-03       100E+06       65.37       557E+8       000E+00       354E-03       100E+06       557E+8       000E+00       354E-03       100E+06       557E+8       000E+00       354E-03       100E+06       557E+8       000E+00       354E-03       100E+06       557E+8       000E+00       354E-03       154E+06       65.37       557E+8       000E+00       354E-03       154E+06       65.37       557E+48       000E+00       354E-03       154E+06       65.37       557E+48       000E+00       354E-03       154E+06       65.37       557E+0       000E+00       354E-03       154E+06       65.37       557E+48       000E+00       154E+06       65.37       557E+48       000E+00       154E+06       65.37       557E+0       357E+02       357E+04       552E-03       154E+06       65.27 </td <td>2200</td> <td>.W/4E+16</td> <td>105E+17</td> <td>48/E+15 552E+15</td> <td>000E+00</td> <td>4438-06</td> <td>2315+03</td> <td>151.60</td> <td>0008+00</td> <td>44.0</td> <td>3008+19 1005+26</td> <td>.815E+19 961E+19</td> <td>-445E+18 506E+18</td> <td>000E+00</td> <td>460E-03</td> <td>800E+05</td> <td>65.17</td> <td>462E-02 \$22E-02</td>	2200	.W/4E+16	105E+17	48/E+15 552E+15	000E+00	4438-06	2315+03	151.60	0008+00	44.0	3008+19 1005+26	.815E+19 961E+19	-445E+18 506E+18	000E+00	460E-03	800E+05	65.17	462E-02 \$22E-02
12000       H31E+17       J32E+17       J32E+16       J32E+17	215.0	.125E+17	.18E+17	.627E+15	.000E+00	.571E-06	.262E+03	151.30	.000E+00	42.0	.115E+20	.199E-20	.576E+18	000E+00	.524E-03	104E+06	65.97	.592E-02
2050       MS2E+17       JSEE+17       SIE+15       OODE+00       SIE+06       337E+06       337E+03       IOS2       OODE+00       SIE+06       SIE+06       SIE+06       SIE+06       SIE+06       SIE+07       ISEE+17       JSEE+17       JSEE+17       JSEE+17       JSEE+17       JSEE+17       JSEE+17       JSEE+17       JSEE+17       JSEE+16       OODE+00       SIE+06       A38E+03       IOOE+00       JSEE+07       JSEE+17       JSEE+17       JSEE+16       JSEE+17       JSEE+16       OODE+00       SIE+17       JSEE+16       OODE+00       SIE+17       JSEE+16       OODE+00       SIE+17       JSEE+17       JSEE+16       OODE+00       SIE+17       JSEE+16       OODE+00       SIE+17       JSEE+16       OODE+00       SIE+17       JSEE+17       JSEE+16       OODE+00       SIE+17       JSEE+17       JSEE+17       JSEE+17       JSEE+16       OODE+00       SIE+17       JSEE+17	210.0	.143E+17	.135E+17	J13E+15	.000E+00	.649E-06	.297E+03	150.98	.000E+00	40.0	.131E+20	.124E+20	.653E+18	.000E+00	.594E-03	.119E+06	66.37	.665E-02
2000       J35E+17       JX6E+17       JX6E+16       JX6E+17	205.0	.152E+17	_15+E+17	811E+15	.000E+00	.738E-06	.337E+03	150.62	.000E+00	380	_148E+20	.140E-20	.739E+18	000E+00	.572E-03	135E+06	66.88	744E-02
1984       1996-17       1981+77       1981+77       1981+76       3000E+00       3930-06       405E+03       190.91       3000E+00       34.0       191E+20       301E+20       301E+20       300E+00       300E+00       300E+00       300E+00       300E+00       300E+00       300E+00       984E+06       407E+03       199.91       000E+00       302       21E+20       21E+20       101E+20       301E+10       000E+00       984E+06       67.77       107E+00         192.0       228E+17       21E+17       108E+16       000E+00       102E-03       32E+02       13E+20       13E+20       300E+00       12E+02       23E+16       000E+00       12E+03       13E+01         190.0       240E+17       228E+17       14E+16       000E+00       12E+03       32E+07       104E+0       300E+00       12E+02       23E+16       000E+00       12E+03       32E+07       104E+0       30E+02       33E+17       30E+02       33E+17       30E+17       32E+17       13E+16       000E+00       12E+03       32E+03       1042       30E+03	200.0	.185E+17	.17KE+17	.924E+15	.000E+00	.841E-06	.383E+03	150.23	.000E+00	360	_168E+20	.160E-20	.840E+18	000E+00	.764E-03	.154E+06	67.14	.84IE-02
194.9       216E+17       205E+17       108E+16       000E+00       3042+03       447E+03       149.74       000E+00       2302+20       122E+19       000E+00       11E+02       228E+06       68.30       120E+01         190.0       2408+17       222E+17       104E+16       000E+00       109E+05       496E+03       149.37       000E+00       260       31E+20       138E+19       900E+00       142E+02       235E+06       68.87       13+E-01         1840       240E+17       228E+17       108E+16       000E+00       125E+05       532E+03       149.21       000E+00       240       356E+20       135E+10       145E+0       235E+06       68.87       13+E-01         1840       266E+17       24E+17       124E+16       000E+00       122E+03       130E+03       149.21       000E+00       240       356E+20       135E+05       696E+07       71.54       178E+01         1840       262E+17       248E+17       148E+16       000E+00       122E+03       148.56       000E+00       140E+20       371E+20       271E+19       000E+00       274E+02       321E+17       146E+16       73.48       21450         1840       331E+17       331E+17       331E+17       331E+17	198.0	.195E+17	.180E+17	374E+15 .103E+16	.000E+00	.933E-06	.403E+03 .425E+03	149.91	.000E+00	34.0	.191E+20 .216E+20	.BIE+20 .206E+20	.108E+19	000E+00	.984E-03	.170E+06 .200E+05	67.38	.107E-01
Prime       Prime <th< td=""><td>104.0</td><td>165.12</td><td>306E 117</td><td>MREIN</td><td>00000-000</td><td>05472.04</td><td>4475 . 02</td><td>10.77</td><td>00012 : 00</td><td>300</td><td>2455 . 22</td><td>22215 - 22</td><td>12212-110</td><td>00015 100</td><td>INF OD</td><td>20851.05</td><td>68 10</td><td>1705 02</td></th<>	104.0	165.12	306E 117	MREIN	00000-000	05472.04	4475 . 02	10.77	00012 : 00	300	2455 . 22	22215 - 22	12212-110	00015 100	INF OD	20851.05	68 10	1705 02
1000       240E+17       228E+17       120E+16       000E+00       140E+03       149.39       000E+00       120E+03       140E+03	199.0	.210E+17	200E+17	114E+16	000E+00	.984E-06	4718-403	149.74	000E+00	280	235E+20	253E+20	138E+19	000E+00	126E-02	2598+05	68.81	134E-01
	190.0	.240E+17	.228E+17	.120E+16	.000E+00	.109E-05	.496E+03	149.39	.000E+00	260	.311E+20	.296E+20	.156E+19	000E+00	.142E-02	295E+06	69.62	.148E-01
186.6       267E+17       254E+17       134E+16       000E+00       122E-05       .530E+03       149.03       000E+00       220       391E+20       .96E+19       000E+00       .178E-02       379E+06       71.54       .178E-01         186.0       .262E+17       .236E+17       .191E+16       .000E+00       .135E+05       .60E+103       148.66       000E+00       .200E+02       .230E+00       .230E+05       .230E+05       .24E+01         180.0       .314E+17       .268E+17       .157E+16       .000E+00       .135E+05       .60E+103       148.66       .000E+00       .180       439E+20       .47E+20       .237E+19       .000E+00       .227E+02       .44E+06       .73.48       .24E+01         176.0       .350E+17       .35E+17       .165E+16       .000E+00       .159E+05       .73E+03       148.26       .000E+00       140       .604E+20       .37E+20       .302E+19       .000E+00       .275E+02       .618E+06       .76.05       .250E-01         176.0       .350E+17       .351E+17       .15E+16       .000E+00       .159E+05       .74E+03       147.87       .000E+00       .304E+20       .370E+20       .370E+19       .000E+00       .304E+02       .56E+06       .73.48       .24E+06	188.0	.254E+17	.24IE+17	.127E+16	.000E+00	.II5E-05	.522E+03	149.21	.000E+00	24.0	350E+20	.332E+20	.175E+19	,000E+00	.159E-02	335E+06	70.48	.165E-01
184.0       .382E+17       .248E+17       .248E+16       .000E+00       .200E+05       .200E+05       .200E+05       .200E+05       .200E+05       .200E+05       .221E+01         182.0       .298E+17       .283E+17       .283E+17       .283E+17       .285E+17       .157E+16       .000E+00       .135E+05       .60E+03       148.66       .000E+00       .200E+20       .245E+19       .000E+00       .223E+02       .486E+05       .74.8       .214E+01         178.0       .331E+17       .15E+16       .000E+00       .151E+05       .678E+03       148.46       .000E+00       .016       .544E+20       .372E+19       .000E+00       .237E+02       .688E+06       .76.05       .250E+01         178.0       .331E+17       .15E+16       .000E+00       .151E+05       .75E+03       148.06       .000E+00       .12.0       .669E+20       .574E+20       .302E+19       .000E+00       .304E+02       .575E+06       .68.8       .200E+01       .304E+02       .575E+06       .68.8       .68.2       .290E+01       .200E+00       .304E+02       .500E+00       .304E+02       .500E+00       .304E+02       .500E+00       .304E+02       .500E+00       .304E+02       .500E+00       .304E+02       .500E+00       .308E+01       .200E+00<	186.0	.267E+17	.254E+17	.134E+16	.000E+00	.122E-05	.550E+03	149.03	.000E+00	22.0	.39IE+20	.371E+20	_196E+19	.000E+00	.178E-02	379E+06	71.54	.178E-01
1820       332E+17       349E+17       349E+17       349E+17       349E+17       352E+17       352E+16       000E+00       148.6       000E+00       148.6       000E+00       140       644E+20       574E+20       302E+19       000E+00       275E-02       618E+06       76.05       250E-01         174.0       369E+17       352E+17       352E+16       000E+00       159E-05       715E+03       148.06       000E+00       120       669E+20       335E+19       000E+00       304E-02       782E+06       78.82       290E-01         174.0       369E+17       375E+17       375E+16       000E+00       187E-05       795E+03       147.67       000E+00       1772E+02       772E+20       370E+19       000E+00       370E-02       877E+06       80.51       308E+01         170.0       412E+17       370E+17       370E+17       230E+16       000E+00       1370E-02       833E+20       440E+19	184.0	.282E+17	.268E+17	.141E+16	.000E+00	.128E-05	.529E+03	148.85	00+3000.	200	4398+20	.417E-20	.219E+19	000E+00	.2008-02	430E+05	72.33	197E-01
1780       331E+17       30E+17       30E+17       30E+16       000E+00       151E+05       678E+03       143.6       000E+00       151E+05       678E+03       143.6       000E+00       120       604E+20       574E+20       302E+19       000E+00       275E+02       618E+06       76.05       250E+01         174.0       369E+17       332E+17       375E+16       000E+00       159E+05       715E+03       148.66       000E+00       120       669E+20       334E+19       000E+00       304E-02       696E+01       77.39       270E+01         174.0       369E+17       351E+17       385E+16       000E+00       168E+05       754E+03       147.67       000E+00       120       669E+20       334E+19       000E+00       336E-02       782E+06       78.82       290E+01         172.0       390E+17       370E+17       395E+16       000E+00       187E+05       388E+03       147.43       100E+04       50       932E+20       388E+20       348E+10       300E+04       50       932E+20       388E+19       000E+00       304E+05       8338±01       147.25       100E+04       50       932E+20       388E+20       510E+07       8333       8332E+01       100E+07       8432+342E+01       100E+04	180-0	.190E T17	298E+17	157E+16	000E+00	.135E-05	643E+03	148.46	000E+00	160	544E+20	97E-20	272E+10	000E+00	243E-02	400E-T00 549E-+05	74.75	231E-01
1760       350E+17       332E+17       375E+16       000E+00       159E-05       715E+03       148.06       000E+00       120       669E+20       636E+20       335E+19       000E+00       304E-02       696E+01       77.39       .270E+05         174.0       369E+17       .351E+17       .185E+16       .000E+00       .168E+05       .74E+03       147.67       .000E+00       .069E+20       .370E+19       .000E+00       .336E-02       .782E+06       78.82       .290E+01         172.0       .390E+17       .390E+17       .200E+16       .000E+00       .187E-05       .338E+03       147.45       .000E+04       .80       .814E+20       .732E+20       .406E+02       .981E+06       .80.51       .308E-01         166.0       .435E+17       .40E+17       .218E+16       .000E+00       .187E-05       .838E+03       147.45       .000E+04       .50       .932E+20       .848E+20       .446E+19       .000E+00       .423E+02       .004E+04       .83.33       .334E+01         166.0       .460E+17       .433E+17       .238E+16       .000E+00       .231E+05       .944E+03       .902E+20       .598E+19       .000E+00       .423E+02       .104E+07       .83.33       .334E+01         166.0 <t< td=""><td>178.0</td><td>.33IE+17</td><td>.315E+17</td><td>.166E+16</td><td>.000E+00</td><td>.151E-05</td><td>.678E+03</td><td>148.26</td><td>.000E+00</td><td>14.0</td><td>.604E+20</td><td>_574E+20</td><td>.302E+19</td><td>.000E+00</td><td>.275E-02</td><td>.618E+06</td><td>76.05</td><td>.250E-01</td></t<>	178.0	.33IE+17	.315E+17	.166E+16	.000E+00	.151E-05	.678E+03	148.26	.000E+00	14.0	.604E+20	_574E+20	.302E+19	.000E+00	.275E-02	.618E+06	76.05	.250E-01
174.0       369E+17       .351E+17       .185E+16       .000E+00       .168E-05       .754E+03       147.87       .000E+00       .000E+00       .370E+19       .000E+00       .336E-02       .782E+06       78.82       .290E-01         172.0       .390E+17       .370E+17       .390E+16       .000E+00       .177E-05       .795E+03       147.66       .000E+00       .000E+00       .370E-02       .877E+06       .80.51       .308E-01         170.0       .412E+17       .391E+17       .200E+16       .000E+00       .187E-05       .884E+03       147.43       .000E-04       .60       .893E+20       .448E+10       .406E+02       .981E+06       .82.24       .327E+01         1660       .435E+17       .416E+17       .218E+16       .000E+00       .981E+05       .884E+03       147.43       .000E+04       .50       .932E+20       .848E+20       .446E+19       .000E+00       .421E+06       .83.3       .83.48E+03       147.03       .000E+04       .50       .932E+20       .848E+120       .519E+19       .000E+00       .421E+02       .934E+03       .000E+04       .40       .974E+23       .446E+02       .102E+04       .423E+03       .406E+02       .100E+04       .40       .974E+23       .548E+19       .000E+00 <t< td=""><td>176.0</td><td>.350E+17</td><td>.332E+17</td><td>J75E+16</td><td>.000E+00</td><td>.159E-05</td><td>.7I5E+03</td><td>148.06</td><td>.000E+00</td><td>12.0</td><td>.669E+20</td><td>.636E+20</td><td>.335E+19</td><td>.000E+00</td><td>.304E-02</td><td>.696E+06</td><td>77.39</td><td>.270E-0</td></t<>	176.0	.350E+17	.332E+17	J75E+16	.000E+00	.159E-05	.7I5E+03	148.06	.000E+00	12.0	.669E+20	.636E+20	.335E+19	.000E+00	.304E-02	.696E+06	77.39	.270E-0
172.0       390E+17       370E+17       .995E+16       .000E+00       .177E-05       .795E+03       147.66       .000E+00       .80       .814E+20       .773E+20       .407E+19       .000E+00       .370E-02       .877E+06       .80.51       .308E-01         1700       .412E+17       .391E+17       .200E+16       .000E+00       .187E-05       .838E+03       147.43       .000E+04       .00       .408E+02       .446E+19       .000E+00       .408E+02       .981E+06       .82.24       .327E+06         1660       .435E+17       .218E+16       .000E+00       .187E-05       .838E+03       147.25       .000E-04       .50       .932E+20       .848E+20       .519E+19       .000E+00       .421E-02       .934E+01       .8.33       .334E-01         1660       .465E+17       .237E+16       .000E+00       .221E-05       .944E+03       147.03       .00E-04       .00       .00E+04       .40       .00       .724E+18       .000E+00       .421E+02       .934E+01       .10E+07       .85.65       .346E+01         162.0       .513E+17       .435E+17       .237E+16       .000E+00       .231E+05       .100E+04       146.66       .000E+04       .20       .105E+21       .954E+20       .974E+20	174.0	.369E+17	.35IE+17	.185E+16	.000E+00	.168E-05	.754E+03	147.87	.000E+00	10.0	.740E+20	.703E+20	.370E+19	.000E+00	.336E-02	.782E+06	78.82	.290E-01
1700       .42E+17       .39E+17       .206E+16       .000E+00       .187E+05       .838E+03       147.43       .00E-04       6.0       .893E+20       .848E+20       .446E+19       .000E+00       .406E+02       .961E+06       82.24       .327E+01         1660       .435E+17       .46E+17       .218E+16       .000E+00       .998E+05       .884E+03       147.43       .00E-04       5.0       .932E+20       .848E+20       .519E+19       .000E+00       .423E+02       .104E+07       .83.3       .334E+01         1660       .660       .436E+17       .243E+16       .000E+00       .221E+05       .934E+03       147.03       .00E+04       .00       .974E+20       .518E+19       .00E+00       .404E+02       .10E+07       .83.3       .342E+01         162.0       .513E+17       .435E+17       .257E+16       .000E+00       .231E+05       .104E+04       146.60       .00E+04       .00       .00E+04       .00E+04       .00       .00E+04       .00       .00E+04       .00E+04       .00E+04       .105E+04       .10E+04       .105       .00E+04       .10       .105E+04       .10       .10       .10E+04       .10       .100E+04       .10       .100E+04       .10       .100E+04       .10	172.0	.390E+17	.370E+17	.195E+16	.000E+00	.177E-05	.795E+03	147.66	.000E+00	8.0	.814E+20	.773E+20	.407E+19	.000E+00	.370E-02	.877E+06	80.51	.308E-01
Instruction         4352E+17         416E+17         218E+16         000E+00         938E-05         834E+03         147.25         000E-04         5.0         932E+20         539E+19         000E+00         423E+07         83.33         334E-01           1660         460E+17         437E+17         230E+16         000E+00         209E-05         933E-03         147.03         000E-04         4.0         974E+20         593E+19         000E+00         441E-02         110E+07         84.23         342E-01           364.0         486E+17         461E+17         243E+16         000E+00         231E-05         146.62         100E-04         4.0         974E+20         593E+19         000E+00         441E-02         110E+07         84.23         342E-01           162.0         513E+17         257E+16         000E+00         233E+05         104E+04         146.60         100E-04         2.0         105E+21         991E+20         724E+19         000E+00         468E+02         112E+07         87.39         345E-01           1660         543E+17         51E+17         32E+17         53E+17         50E+04         445.38         100E+04         1.5         100E+04         1.5         100E+21         995E+20         102E+20	170.0	.412E+17	.39IE+17	.200E+10	.000E+00	.187E-05	.838E+03	147.45	.100E-04	6.0	.893E+20	.848E+20	.446E+19	.000E+00	.406E-02	.981E+06	82.24	.327E-01
04:0       340E+17       340E+16       300E+10       300E+00       303E+03       164.0       360E+03       300E+00       300E+03       340E+03       140.3       300E+04       300E+04       300E+00       340E+02       110E+07       84.29       342E+0         164.0       365E+17       366E+17       340E+16       300E+00       23E+05       100E+04       146.02       300E+04       30       300E+21       399E+20       74E+29       300E+00       448E+02       110E+07       85.65       346E-01         162.0       .513E+17       .55E+17       .55E+17 <td< td=""><td>168.0</td><td>.435E+17</td><td>40E+17</td><td>.218E+16</td><td>000E+00</td><td>.198E-05</td><td>884E+03</td><td>147.25</td><td>100E-04</td><td>5.0</td><td>932E+20</td><td>2890E+20</td><td>.519E+19</td><td>000E+00</td><td>423E-02</td><td>.104E+07</td><td>83.33</td><td>.334E-01</td></td<>	168.0	.435E+17	40E+17	.218E+16	000E+00	.198E-05	884E+03	147.25	100E-04	5.0	932E+20	2890E+20	.519E+19	000E+00	423E-02	.104E+07	83.33	.334E-01
162.0         513E+17         488E+17         257E+16         000E+00         233E+05         104E+04         146.66         D00E+04         2.0         105E+21         954E+20         90TE+19         200E+00         464E+02         122E+07         87.39         343E+01           160.0         .543E+17         .5UE+17         .2TE+16         .000E+00         .247E+05         .100E+04         146.38         .000E+04         1.5         .106E+21         .954E+20         .000E+00         .464E+02         .122E+07         .87.39         .344E+01           133.0         .574E+17         .287E+16         .000E+00         .247E+05         .106E+04         146.17         .000E+04         1.5         .106E+21         .959E+20         .100E+21         .900E+00         .473E+02         .122E+07         .89.08         .344E+01           156.0         .606E+17         .578E+17         .303E+16         .000E+00         .276E+05         .122E+04         .145.95         .100E+21         .990E+20         .100E+20         .000E+00         .489E+02         .132E+07         .89.68         .344E+01           154.0         .640E+17         .578E+17         .302E+16         .000E+00         .489E+02         .132E+07         .89.68         .344E+01	106.0	.460E+17	.451E+17	243E+16	000E+00	.2098-05	984E-03	147.03	.100E-04	4.0	JOHE+21	.914E+20 .939E+20	.724E+19	.000E+00	441E-02	.10E+07	8565	.342E-01
1600       .543E+17       .515E+17       .271E+16       .000E+00       .247E-05       .10E+04       .146.38       .00E+04       .15       .106E+21       .959E+20       .102E+20       .000E+00       .473E-02       .122E+07       .88.31       .344E-01         1530       .574E+17       .287E+36       .000E+00       .261E-05       .16E+04       .16.17       .000E+04       .15       .106E+21       .959E+20       .100E+04       .480E-02       .128E+07       .89.31       .344E-01         1560       .606E+17       .578E+17       .303E+16       .000E+00       .276E-05       .122E+04       .145.95       .100E+04       .5       .10E+21       .990E+20       .10E+20       .000E+00       .489E-02       .132E+07       .89.68       .344E-01         154.0       .641E+17       .609E+17       .321E+16       .000E+00       .292E-05       .129E+04       .15.72       .00E-04       .01E+21       .101E+21       .101E+21       .101E+21       .135E+07       .90.29       .350E-04         152.0       .678E+17       .609E+107       .339E+16       .000E+00       .399E+05       .156E+04       .145.40       .00E+04       .01E+21       .112E+20       .000E+00       .498E+02       .135E+07       .90.29       .350E+	162.0	.513E+17	.488E+17	257E+16	.000E+00	233E-05	_104E+04	146.60	.100E-04	2.0	.105E+21	.954E+20	.917E+19	/000E+00	468E-02	.122E+07	87.39	.345E-01
158.0       .574E+17       .267E+16       .00E+00       .261E+05       .16E+04       H6.17       .00E+04       1.0       .106E+21       .571E+20       .106E+20       .000E+00       .480E+02       .12E+07       B9.06       .344E+01         156.0       .606E+17       .578E+17       .303E+16       .000E+00       .276E+05       .122E+04       H5.95       .100E+04       .5       .10E+21       .990E+20       .10E+20       .000E+00       .489E+02       .132E+07       89.68       .344E+01         154.0       .641E+17       .609E+17       .321E+16       .000E+00       .292E+05       .129E+04       H5.72       .00E+04       .01E+21       .112E+20       .000E+00       .498E+02       .135E+07       90.29       .350E+04         152.0       .678E+17       .645E+17       .339E+16       .000E+00       .399E+05       .156E+04       .145.40       .100E+04       .01E+21       .112E+20       .000E+00       .498E+02       .135E+07       .90.29       .350E+04	160.0	.543E+17	.515E+17	.27IE+16	.000E+00	_247E-05	.D0E+04	146.38	.100E-04	1.5	.106E+21	.959E+20	.102E+20	/000E+00	A73E-02	.125E+07	88.31	.344E-01
ISON         SOBE+17         STRE+17         SOBE+16         DODE+00         .276E-05         .122E+04         145.95         .00E-04         .5         .10E+20         .000E+00         .489E-02         .132E+07         89.68         .347E-01           154.0         .641E+17         .609E+17         .321E+16         .000E+00         .292E+05         .129E+04         H5.72         .00E-04         .0         .112E+21         .01E-21         .112E+20         .000E+00         .498E-02         .135E+07         .90.29         .350E-04           152.0         .678E+17         .339E+16         .000E+00         .309E+04         .145.40         .00E-04         .0         .112E+21         .01E-21         .112E+20         .000E+00         .498E-02         .135E+07         .90.29         .350E-04	158.0	_574E+17	.545E+17	.287E+16	.000E+00	.261E-05	.1/6E+04	146.17	.100E-04	1.0	.106E+21	.971E-20	.106E+20	00+3000.	.480E-02	.1282.+07	89.08	.34412-01
154.0 641E+17 609E+17 321E+16 000E+00 292E-05 129E+04 145.72 X0E-04 0 .112E+21 J01E-21 J12E+20 000E+00 498E-02 J35E+07 90.29 350E-04 152.0 678E+17 545E+17 339E+16 000E+00 309E-05 155E+04 145.40 X0E-04	156.0	.606E+17	.576E+17	.303E+16	.000E+00	.276E-05	.122E+04	145.95	.100E-04	.5	.110E+21	.990E+20	.IICE+20	.00+3000.	.489E-02	.132E+07	89.68	.347E-01
	154.0 152.0	.041E+17 .678E+17	.609E+17 .645E+17	.321E+16 .339E+16	.000E+00	.292E-05 .309E-05	.129E+04 .136E+04	145.72 145.49	.100E-04 .100E-04	.0	.II2E+21	.DIE-21	.H2E+20	.000E+00	.498E-02	.135E+07	90.29	.350E-01

Table 5. Maximum Yelle model for Titan's atmosphere. CH<sub>4</sub> 1%, Ar 10%, N<sub>2</sub> 89%, mean mass 28.72, T(1) = 175.0, T(2) = 134.0, T(3) = 174.0,  $\kappa = 0.500$ , A<sub>1</sub> = 0.009, A<sub>2</sub> = 0.001, A<sub>3</sub> = 0.100, Z<sub>h</sub> = 830.0.

Z	Nu	mber Der	sities (cm	3	Mass	Pressure	Temp	F	7	Number Densities (cm <sup>3</sup> )		Mass	Processo	Town	F		
(km)	Total	N	CH	Ar	(gm/cm <sup>3</sup> )	(org/cm <sup>3</sup> )	(K)	С. P.	(km)	Total	N	CH	Ar	(em/cm <sup>3</sup> )	(erg/cm <sup>3</sup> )	(K)	· e
-		- 1		17-10-21-51-85			1000	COLUMN THE	(read)	10101	2	1		Bunery 1	(e.g.c.n.)	prey.	
1300.0	.383E+10	_324E+10	.529E+09	.569E+08	.168E-12	.108E-03	204.00	.000E+00	890.0	.332E+12	.306E+12	.702E+10	.188E+11	155E-10	.930E-02	203.22	.000E+00
1295.0	.400E+10	.341E+10	_541E+09	.606E+08	.177E-12	.113E-03	204.00	.000E+00	885.0	.353E+12	.326E+12	.735E+10	.204E+II	.166E-10	.990E-02	202.99	.000E+00
12850	441E+10	377E+10	555E+09	680E+08	105E-12	124E-03	204.00	000E+00	880.0	.377E+12 403E+13	347E+12	770E+10	220E+II	177E-10 180E 10	NOSE-OL	202.75	.000E+00
1280.0	.462E+10	.397E+10	_580E+09	.735E+08	204E-12	.130E-03	204.00	.000E+00	870.0	4298+12	395E+12	346E+10	256E+II	201E-10	1205-01	202.47	000E+00
1275.0	.485E+10	.417E+10	.594E+09	.784E+08	.214E-12	.136E-03	204.00	.000E+00	865.0	458E+12	.421E+12	.888E+10	.278E+II	.215E-10	.128E-01	201.85	.000E+00
1270.0	.508E+10	.439E+10	.608E+09	.836E+08	.225E-12	.143E-03	204.00	.000E+00	860.0	.489E+12	A50E+12	.932E+10	.300E+11	.230E-10	.136E-00	201.50	.000E+00
12650	.533E+10	.462E+10	.622E+09	.892E+08	237E-12	.150E-03	204.00	.000E+00	855.0	.523E+12	.480E+12	,979E+10	.325E+11	.245E-10	.145E-01	201.13	.000E+00
12550	.339E+10 587E+10	-450E+10 5/2E+10	038E+09 653E±00	.952E+08	.249E-12 261E-12	.158E-03	204.00	000E+00	850.0	.559E+12	513E+12	103E+11	.352E+II	.263E-10	.155E-0	200.73	.000E+00
12350	120/12/10	-31213+10	0000-+09	.1022.709	.2016-12	-1036-03	204.00	10008+00	845.0	3965+12	349E+12	.108E+II	.38/E+II	_281E-10	. HOSE-OI	200.90	100E+00
12500	.616E+10	_539E+10	.669E+09	.109E+09	.275E-12	.174E-03	204.00	.000E+00	840.0	.639E+12	.587E+12	.11482+11	.412E+II	.301E-10	.176E-01	199.86	.0002+00
1245.0	.647E+10	.567E+10	,6868+09	.116E+09	.289E42	.182E-03	204.00	.000E+00	835.0	/584E+12	628E+12	.120E+II	_446E+1I	.322E-J0	.188E-00	199.39	.000E+00
12400	.679E+10	.597E+10	.703E+09	.124E+09	_304E-12	.191E-03	204.00	.000E+00	830.0	.733E+12	.672E+12	.127E+II	_484E+1	.345E-10	.201E-01	198.90	.000E+00
12350	-7148+10	.028E+10	721E+09	132E+09	.399E-12	.201E-03	204.00	.000E+00	825.0	.786E+12	.720E+12	_134E+11	.524E+11	.370E-10	.215E-00	158.38	.000E+00
12250	788E+10	607E+10	759E+09	15 F + 09	3536-12	222E-03	204.00	000000000	8200	.842E+12 004E+17	\$27E+12	14012 + 11	-368E+11	.397E-10	246E-01	197.85	0008+00
12200	.828E+10	.734E+10	.777E+09	16IE+09	.371E-12	233E-03	204.00	000E+00	800	.904E+12	887E+12	158E+0	669E+1	457E-10	263E-01	196.71	000E+00
1215.0	.870E+10	.773E+10	.798E+09	.173E+09	.391E-12	.245E-03	204.00	.000E+00	805.0	.104E+13	.952E+12	.167E+11	.726E+11	.491E-10	282E-01	196.12	.000E+00
1210.0	.914E+10	.8I4E+10	818E+09	.185E+09	.411E-12	.257E-03	204.00	.000E+00	800.0	.112E+13	.102E+13	.177E+II	.788E+11	.527E-03	302E-01	195.50	.000E+00
1205.0	.961E+10	.858E+10	.840E+09	.197E+09	.433E-12	.271E-03	204.00	.000E+00	795.0	.120E+13	.110E+13	.188E+11	855E+II	.567E-10	323E-01	194.86	1000E+00
12000	101E+11	904F110	862E±00	2016±09	4568-12	2855-03	204.00	0008+00	790.0	120E+13	1992-113	2006-11	9766-11	6015-00	3475.01	194.20	0008-100
1195.0	.106E+11	.952E+10	.885E+09	.226E+09	480E-12	.299E-03	204.00	.000E+00	785.0	.139E+13	127E+13	212E+1	.101E+12	.657E-10	372E-01	193.52	_000E+00
1190.0	.112E+11	.100E+11	.909E+09	.242E+09	.505E-12	.315E-03	204.00	.000E+00	780.0	.150E+13	.137E+13	.226E+II	.HOE+12	.708E-10	399E-01	192.83	.000E+00
11850	.HSE+H	.106E+11	.933E+09	.259E+09	_532E-12	.331E-03	204.00	.000E+00	775.0	_162E+13	.147E+13	.240E+11	.119E+12	.763E-10	.428E-0I	192.12	.000E+00
1180.0	.124E+11	-112E+11	.959E+09	.277E+09	.561E-12	.349E-03	204.00	.000E+00	770.0	.174E+13	.159E+13	.256E+II	.130E+12	.823E-10	.460E-01	191.39	.000E+00
1175.0	.130E+11	.118E+11	.985E+09	_297E+09	.591E-12	.367E-03	204.00	.000E+00	765.0	_188E+13	.171E+13	.273E+11	.142E+12	.888E-10	.495E-01	190.65	.000E+00
11650	137E+11	131E+11	104E+10	341E+09	6568-12	.387E-03	204.00	000E+00	760.0	203E+13	100E+12	291E+11 310E+11	1048+12 169E+12	104E-00	57212-01	189.89	0005+00
1160.0	.152E+11	.138E+11	.107E+10	365E+09	691E-12	4296-03	204.00	.000E+00	750.0	237E+13	215E+13	.332E+0	183E+12	.112E-09	66E-0	189.12	000E+00
11550	.160E+11	.145E+11	.1108+10	.39(E+09	.7298-12	.452E-03	204.00	.000E+00	745.0	.256E+13	.233E+13	.355E+II	.200E+12	.121E-09	.063E-OI	187.53	.000E+00
				and a second second													
11500	.169E+11	.153E+11	.113E+10	419E+09	.769E-12	.476E-03	204.00	000E+00	740.0	.277E+13	252E+13	.380E+II	.218E+12	.13IE-09	.714E-01	186.72	000E+00
1140.0	188E+11	171E+11	120E+10	482E+09	855E-12	.501E-03	204.00	000E+00	730.0	325E+13	205E+13	437E+1	260E+12	154E-09	831E-01	185.07	000E+00
1135.0	.198E+11	.180E+11	123E+10	SITE+09	.902E-12	.557E-03	204.00	.000E+00	725.0	353E+13	.320E+13	469E+11	.284E+12	.167E-09	897E-01	184.23	.000E+00
1130.0	.209E+11	.190E+11	.127E+10	.554E+09	.952E-12	.587E-03	204.00	.000E+00	720.0	.383E+13	347E+13	.504E+11	.310E+12	.181E-09	.969E-01	183.38	.000E+00
11250	.220E+II	.201E+11	.131E+10	.595E+09	.100E-11	.619E-03	204.00	.000E+00	715.0	.416E+13	.376E+I3	.542E+il	.339E+12	.197E-09	.105E+00	182.53	.000E+00
1120.0	.232E+II	.212E+11	134E+10	,638E+09	.106E-11	.653E-03	204.00	.000E+00	710.0	452E+13	.409E+13	584E+11	.37IE+12	_214E-09	.113E+00	181.67	.000E+00
1115.0	.245E+11	.224E+11	.138E+10	,685E+09	.112E-11	.689E-03	204.00	.000E+00	705.0	.491E+13	.444E+13	.629E+11	.406E+12	.233E-09	.123E+00	190.90	.000E+00
1000	.258E+II 27372+II	2508-11	.143E+10	733E+09	198E-11	727E-03	204.00	000E+00	700.0	5936+13	483E+13	/079E+II	.443E+12 .497E+13	2336-09	,133E+00	179.94	000E+00
110,50	.212671	.2006 11	TALETIN	1096709	4626-0	10/12-03	204.00	20005-00	093.0	13046713	2005-13	2226714	,90/GT14	-2706-09		175.07	
1100.0	.288E+11	.264E+11	.151E+10	.847E+09	.B2E-II	.810E-03	204.00	.000E+00	690.0	,634E+13	.572E+13	.792E+11	.534E+12	.300E-09	.156E+00	178.21	.000E+00
1095.0	.304E+11	.279E+11	.156E+10	.909E+09	.139E-11	.855E-03	204.00	.000E+00	685.0	.691E+13	624E+I3	.856E+11	.586E+IZ	.328E-09	.169E+00	177.35	.000E+00
1090.0	_321E+11	.295E+11	.161E+10	.976E+09	,147E-11	.903E-03	204.00	.000E+00	680.0	.754E+13	680E+13	.927E+11	.643E+12	.357E-09	.184E+00	176.49	.000E+00
1085.0	.339E+II	.312E+11	166E+10	.105E+10	.156E-II	.953E-03	204.00	.000E+00	675.0	.823E+13	.742E+13	.100E+12	.706E+12	.390E-09	.199E+00	175,64	000E+00
1025.0	3788 + 11	3488+11	177E+10	12(E+10	1745-11	10(E-02 106E-02	204.00	000E+00	665.0	082E+13	885E+13	118E+12	852E+12	466E-09	236E+00	171.07	100E+00
1070.0	.399E+1	.368E+11	.182E+10	130E+10	.184E-11	.112E-02	204.00	.000E+00	660.0	.107E+14	.968E+13	.128E+12	.937E+12	-510E-09	.257E+00	173.15	.000E+00
1055.0	.422E+II	.389E+II	.188E+10	.140E+10	.194E-11	.119E-02	204.00	.000E+00	655.0	.118E+14	.106E+14	.140E+12	.103E+13	.558E-09	_280E+00	172.35	.000E+00
1050.0	.446E+11	.4I2E+11	.194E+10	.150E+10	.206E-11	.126E-02	204.00	.000E+00	650.0	_129E+14	.116E+14	.152E+12	.113E+13	.611E-09	_305E+00	171.57	.000E+00
1055.0	.472E+11	.435E+11	.201E+10	.162E+10	.218E-11	.133E-02	204.00	.000E+00	645,0	_141E+14	.127E+14	,165E+12	.125E+13	.670E-09	_333E+00	170.80	.000E+00
10500	490E+1	461E+11	208E+10	DAR+D	2306-0	1408-02	204.00	000E+00	6400	155E+14	139E+14	180E+12	137E+13	734E-09	163E+00	170.06	000E+00
1045.0	528E+1	.487E+11	214E+10	187E+10	.244E-11	.149E-02	204.00	.000E+00	635.0	.170E+14	153E+14	.196E+12	.15IE+13	805E-09	.396E+00	169.35	.000E+00
1040.0	558E+11	.516E+11	.222E+10	.201E+10	.258E-11	.157E-02	204.00	.000E+00	630.0	.186E+14	.167E+14	.214E+12	.167E+13	.884E-09	.433E+00	168.67	.000E+00
10350	_591E+11	.546E+11	.229E+10	.216E+10	.273E-II	.166E-02	204.00	.000E+00	625.0	.204E+14	184E+14	.234E+12	.184E+13	.971E-09	_474E+00	168.02	000E+00
1030.0	.625E+11	.578E+11	.237E+10	.233E+30	.289E-II	.I76E-02	204.00	.000E+00	620.0	.224B+14	.202E+14	.256E+12	.203E+13	.107E-08	.519E+00	167.40	.000E+00
1025.0	.662E+11	.612E+11	.245E+10	.250E+10	.306E-II	.186E-02	204.00	.000E+00	615.0	247E+14	221E+14	.280E+12	.224E+B	.117E-08	_568E+00	166.83	.000E+00
10150	742E+11	.0486E+11	263E+10	290E+10	3446-11	2098-02	204.00	000E+00	605.0	2988+14	267E+14	335E+12	273E413	1428-08	682E+00	165.81	0005+00
10000	.785E+11	.727E+11	.272E.410	312E+10	.364E-11	.221E-02	204.00	.000E+00	600.0	.328E+14	294E+14	.366E+12	.301E+13	156E-08	348E+00	165.37	000E+00
1005.0	.832E+11	.770E+11	.282E+10	_336E+10	.386E-II	.234E-02	204.00	.000E+00	595.0	.361E+14	.323E+14	.401E+12	.332E+13	.171E-06	.821E+00	164.99	.000E+00
10000	0017 - 11	dig	-	2617 - 12	1005.11	0.407 40	004.00	0000 - 00	500.0	2070 111	2665	1305	1670 . 17	1602 05	0015 - 00	164.00	0005 .00
005.0	38IE+II	310E+11	292E+10	.301E+10	.409E-II	2488-02	204.00	000E+00	590.0	.397E+14	300E+14	43912+12	.36/E+13	.189E-08	.90(E+00	164.00	000E+00
9950	.99012+11	.907E-10	348+10	41912+10	4600-11	22058-02	204.00	000E+00	5800	480E+14	430E+14	-528E+12	.400E+13	228E-08	109E+00	164.20	000E+00
985.0	.105E+12	.972E+11	.326E+10	.451E+10	.488E-11	.295E-02	204.00	.000E+00	575.0	.529E+14	.473E+14	.578E+12	.493E+13	-251E-08	.120E+01	164.06	.000E+00
980.0	.IIIE+12	.103E+12	.338E+10	.485E+10	.517E-11	.3I3E-02	204.00	.000E+00	570.0	.582E+14	.521E+14	.634E+12	.544E+13	.277E-08	.132E+01	164.00	.000E+00
975.0	.118E+12	.109E+12	.351E+10	.524E+10	.549E-II	.332E-02	204.00	.000E+00	565.0	.640E+14	.573E+I4	.695E+12	.600E+13	.304E-08	.345E+01	164.03	.000E+00
970.0	.125E+12	.186E+12	.364E+10	.564E+10	.582E-11	.352E-02	204.00	.000E+00	560.0	.704E+14	630E+14	.762E+12	.662E+13	.335E-08	159E+01	164.16	.000E+00
965.0	.153E+12	123E+12 120E+12	378E+10	A08E+10	.618E-11	.374E-02	204.00	.000E+00	555.0	.773E+14	092E+14 260E+14	834E+12 014E+12	.729E+13	308E-08	175E+0	164.40	000E+00
955.0	150E+12	.138E+12	.409E+10	206E+10	.697E-II	.421E-02	204.00	D00E+00	545.0	.933E+14	835E+14	.00E+13	.884E+13	.444E-08	_213E+01	165.18	.000E+00
3.2.0	Sheer Store	128826-0110-	Constantine State	Versioner	10000000	100000000	1055.00	1000000000	0.000	200001112	1000000000	Sector Sector	2012/01/02/02	100000000000000000000000000000000000000	and a second	10000	Supervision .
950.0	159E+12	.147E+12	425E+10	.760E+10	.740E-11	.447E-02	204.00	.000E+00	540.0	.102E+15	.916E+14	.109E+13	.972E+13	.487E-08	.234E+01	165.72	000E+00
945.0	169E+12	.156E+12	.442E+10	320E+10	.766E-II	.475E-02	204.00	.000E+00	535.0	.112E+15	100E+15	.E20E+B	.107E+14	.535E-08	-258E+01	166.34	D00E+00
940,0	1008+12	176E+12	400E+10	951E+10	835E-II 889E II	535E 02	204.00	000E+00	530.0	1358-15	1715 - 15	1316+13	17997-14	580E-08	3128-01	167.83	000E+00
9300	202E+12	1878+12	498E+10	103E+1	.943F-11	569E-02	204.00	000E+00	5200	148E+15	132E+15	.156F+13	141E+14	703E-08	344E+0	168.67	000E+00
925.0	215E+12	.198E+12	_519E+10	.111E+11	.100E-10	.604E-02	204.00	000E+00	515.0	.162E+15	145E+15	.171E+13	.155E+14	770E-08	.378E+01	169.58	.000E+00
920.0	_228E+12	-211E+12	.541E+10	.11915+11	.107E-10	.642E-02	203.97	.000E+00	510.0	.177E+15	.158E+15	.186E+13	.170E+14	.842E-08	.416E+01	170.55	.000E+00
915.0	_243E+12	.224E+12	.564E+10	.129E+II	.H3E-10	.683E-02	203.91	.000E+00	505.0	.193E+15	.173E+15	.203E+13	.186E+14	.921E-08	.458E+01	171.58	.000E+00
910.0	.258E+12 275E+12	.238E+12	.589E+10	139E+II 150E + II	.121E+10	.726E-02	203.83	000E+00	500.0	.211E+15	.189E+15	.722E+13	223E+14	101E-07	.304E+01	172.65	000E+00
9030	.2/30+12	12330+12	0000+10	100240	.m90-10	.11215-02	20332	300000+000	4930	-2316+13	2006 113	16415 T 15	ACCEPT PA	-100-00	10046.100	113.77	UNUE TUR
900.0	.292E+12	.270E+12	.642E+10	.162E+11	.137E-10	.821E-02	203.58	.000E+00	490.0	.252E+15	.225E+15	.263E+13	.244E+14	.120E-07	.609E+01	174.92	.000E+00
895.0	.311E+12	.287E+12	.67IE+10	.175E+11	.146E-10	.874E-02	203.41	.0008+00			-		_	-	C9	nutinued o	n next page

Table 5. (Continued).

-			_	4								-3					
Z	Nu	mber Der	isities (cm	0	Mass	Pressure	Temp	F	Z	Ns	omber Den	sities (cm	")	Mass	Pressure	Temp	F
(km)	Total	N,	CH	Ar	(gm/cm <sup>2</sup> )	(erg/cm <sup>2</sup> )	(K)	100	(km)	Total	N.	CH	Ar	(gm/cm <sup>2</sup> )	(erg/cm <sup>2</sup> )	(K)	
-			•								2	4					
485.0	.275E+15	.246E+15	.287E+13	.267E+14	.131E-07	.669E+01	176.11	.000E+00	150.0	.155E+I8	.138E+18	.156E+16	,156E+17	J42E-05	.390E+04	181.54	.100E-04
480.0	.300E+15	_258E+15	.312E+13	.29IE+I4	.143E-07	.734E+01	177.32	.000E+00	148.0	,163E+18	.145E+18	.163E+16	.163E+17	.779E-05	.408E+04	181.03	,100E-04
475.0	.327E+15	.292E+15	.340E+13	.318E+14	.156E-07	806E+01	178.56	.000E+00	146.0	.172E+18	.153E+18	.172E+16	.172E+17	.822E-05	.428E+04	179,68	.200E-04
470.0	.357E+15	.308E+15	.370E+13	.347E+14	.1708-07	385E+00	179.81	.000E+00	144.0	.180E+18	.160E+18	.180E+16	.190E+17	859E-05	.448E+04	180.12	200E-04
465.0	.389E+15	347E+15	.402E+13	.378E+14	.185E-07	.971E+01	181.08	.000E+00	142.0	.1918+18	170E+18	3915+10	1916+17	.906B-05	469E + 04	178.37	2008-04
4600	443E+15	4112 - 15	43/E+13 476E+13	415B+14	2021-07	1066+02 107E+02	182.30	000E+00	1900	2015-10	1000 10	2018 + 16	2015+17	3012-03	492E 104	177.09	2008-04
433.0	SUDE 115	A47E 115	413E+13	400E+14	22000.07	1285 102	183.07	000E+00	136.0	22212.119	1005+10	2116+10	2235.117	1068.04	5418+04	176.22	2008-04
4450	SAGE +15	487E+15	56/E+13	534E±14	259E-07	1406.402	186.20	000E+00	134.0	2230+18 234E±18	208E+18	234E+16	134E417	1176-04	568E+04	175.90	2005.04
440.0	SQ4F 115	510E+15	60E+13	587E+14	283E-07	154E+02	187.47	000E+00	132.0	247E+18	220E+18	247E+16	747E+17	118F-04	506F+04	175.11	200E-04
	10,000,000		3352.10	Contra 114	TRADE OF	10.462 - 64	101247	100002.100	1000		100000100	18-118-199					2002232024
435.0	:646E+15	.576E+15	.663E+13	633E+14	.308E-07	.168E+02	188.74	:000E+00	130.0	.259E+18	.23IE+18	.259E+16	.259E+17	124E-04	.626E+04	174.82	.200E-04
430.0	.702E+15	.626E+15	.720E+13	689E+14	.335E-07	.184E+02	189.99	.000E+00	128.0	.274E+18	.244E+18	.274E+16	_274E+17	.131E-04	.657E+04	173.44	.300E-04
425.0	.764E+15	.681E+15	.782E+13	.750E+14	.364E-07	.202E+02	191.22	.000E+00	126.0	.291E+18	.259E+18	.291E+16	.291E+17	.139E-04	.690E+04	171.96	.300E-04
420.0	.830E+15	.740E+15	.849E+13	_816E+14	.396E-07	.220E+02	192.43	.000E+00	124.0	_307E+18	.273E+18	.307E+16	_307E+17	146E-04	.725E+04	171.13	.300E-04
415.0	.903E+15	805E+15	.922E+13	.888E+14	.430E-07	_241E+02	193.62	.000E+00	122.0	.326E+18	.290E+18	.326E+16	.326E+17	.155E-04	.762E+04	169.58	.300E-04
410.0	.981E+15	.875E+15	.100E+14	.966E+14	.468E-07	.264E+02	194.78	.000E+00	120.0	.344E+18	306E+18	.344E+16	.344E+17	.164E-04	.802E+04	168.69	.300E-04
405.0	.107E+10	.951E+15	.109E+14	.105E+15	.508E-07	.288E+02	195.92	.000E+00	118.0	.304E+18	.324E+18	.304E+10	.3048+17	174E-04	.843E+04	167.08	A01E-04
400.0	.110E+10	.HUSE+ID	.118E+14	.114E+15	.552E-07	.315E+02	197.02	.000E+00	116.0	.385E+18	.343E+18	.385E+16	.3855+17	184E-04	.888E+04	166.98	401E-04
395.0	1275-116	1226+30	1286+14	1246+15	.600E-07	.344E+02	195.09	.000E+00	114.0	437E+18	204E 119	427E+16	4075+17	194E-04	084E+04	165.10	4012-04
3900	10/6+10	1226+10	.1.9E+14	.135E+D	.055E-07	3708-102	199711	1000E+00	1230	,432E+18	004E+18	,4320+10	(432D/HI)	-200E-04	.9846.404	103.10	.401E-04
385.0	149E+16	133E±16	151E+14	147E+15	2016-00	4116 +02	200.10	000E+00	100	458E+18	407E+18	458E+16	458E+17	218E-04	104E+05	164.17	499E-04
380.0	162E416	144E+16	.164E+M	.160E+15	.772E-07	449E+02	201.05	.000E+00	108.0	485E+18	431E.418	4858+16	485E+17	23IE-04	109E+05	163.43	499E-04
375.0	,176E+16	157E+16	179E+14	.174E+15	.839E-07	491E+02	201.95	.000E+00	106.0	514E+18	457E+18	514E+16	.514E+17	.245E-04	.115E+05	162,50	.499E-04
370.0	.191E+16	.171E+16	.194E+14	.189E+15	.912E-07	.536E+02	202,80	000E+00	104.0	.548E+18	.488E+18	.548E+16	.548E+17	.26IE-04	.122E+05	160.78	.600E-04
365.0	.208E+16	.186E+16	.20E+14	.206E+15	.993E-07	.585E+02	203.60	.000E+00	102.0	.583E+18	.519E+18	.583E+16	.583E+17	.278E-04	.128E+05	159,49	.600E-04
360.0	.227E+16	_202E+16	.229E+14	.224E+15	.108E-06	.639E+02	204.35	.000E+00	100.0	.622E+18	.553E+18	.622E+16	.622E+17	.296E-04	.136E+05	157.97	.700E-04
355.0	.247E+16	-220E+16	-250E+14	244E+15	.118E-06	/698E+02	205.01	.000E+00	98.0	.663E+18	.590E+18	.663E+16	.663E+17	.316E-04	.143E+05	156.62	.700E-04
350.0	.269E+16	_240E+16	.272E+14	.267E+15	.128E-06	.762E+02	205.32	.000E+00	96,0	,707臣+18	629E+18	.707E+16	.707E+17	.337E-04	.151E+05	155.20	.800E-04
345.0	.294E+16	.261E+16	.297E+14	.291E+15	_140E-06	.833E+02	205.57	.000E+00	94.0	.757E+18	.674E+18	.757E+16	.757E+17	.361E-04	.160E+05	153.33	.900E-04
340.0	.320E+16	_285E+16	_324E+14	.318E+15	.153E-06	.910E+02	205.76	.000E+00	92.0	.813E+18	.724E+38	.813E+16	.8I3E+17	.388E-04	.T/0E+05	151.19	,100E-03
1226.0	2000.116	1010		2.020.114	NOTE OF	20.12.02	205.00	0000 . 00	000	PROFIL IN	2710T - 10	0707116	111.120	1100.04	HAVE - OF	140.72	1105 02
3300	1970-16	2410-16	206E±14	20002115	1975 06	100E±03	203.90	00000000	880	039E±19	936E ± 19	03901+16	0390 +17	4430.04	10112-05	145.73	1005-03
1250	1190-116	2776+16	417E+14	4160 + 16	100E 06	1092+03	203.99	0008+00	860	100E±10	900E+19	10000 +17	100E+12	4776.04	2020+05	146.55	130E-03
3200	457E+16	407E+16	4618+14	454E+15	218E-06	130E+03	206.03	000E+00	\$4.0	108E+19	965E+18	108E+17	108E+18	517E-04	215E+05	143.56	140E-03
315.0	.500E+16	446E+16	504E+14	497E+15	239E-06	142E+03	205.94	000E+00	\$2.0	.118E+19	105E+19	118E+17	.118E+18	.563E-04	.229E+05	140.21	.160E-03
310.0	.548E+16	.488E+16	.552E+14	_545E+15	.261E-06	.156E+03	205.82	.000E+00	80.0	.129E+19	.115E+19	.129E+17	.129E+18	614E-04	244E+05	137.11	.180E-03
305.0	.601E+16	_535E+16	605E+14	597E+15	.286E-06	.170E+03	205.66	.000E+00	78.0	.141E+19	125E+19	J4IE+17	.141E+18	.672E-04	_260E+05	133.61	.210E-03
300.0	.659E+16	_586E+16	.663E+14	655E+15	.314E-06	.187E+03	205.45	.000E+00	76.0	.154E+19	.137E+19	.154E+17	.154E+18	736E-04	.278E+05	130.39	.240E-03
295.0	.723E+16	.643E+16	.727E+14	.719E+15	.344E-06	.205E+03	205.18	.000E+00	74.0	.170E+19	.151E+19	.170E+17	.170E+18	.809E-04	_298E+05	127.11	.270E-03
290.0	.793E+16	.706E+16	.798E+14	.790E+15	.378E-06	.224E+03	204.88	.000E+00	72.0	.190E+19	.169E+19	.190E+17	.190E+18	.905E-04	.320E+05	122.09	.330E-03
3620	12223705							100000000000	10000					03225752	60267772	11332365	039360
285.0	.872E+16	.776E+16	.877E+14	.868E+15	.416E-06	.246E+03	204.52	.000E+00	70,0	.216E+19	.192E+19	,216E+17	.216E+18	.103E-03	.344E+05	115.68	.410E-03
280.0	.959E+16	.853E+16	.964E+14	.955E+15	.457E-06	.270E+03	204.13	.000E+00	68.0	.246E+19	.219E+19	.246E+17	.246E+18	.IDE-03	.373E+05	109.68	.5208-03
275.0	.105E+17	.939E+16	.106E+15	.105E+16	.503E-06	.296E+03	203.69	.000E+00	65.0	.288E+19	.256E+19	.288E+17	.288E+18	.137E-03	.405E+05	102.18	.080E-03
270.0	_110E+17	.103E+17	.H7E+15	.106E+16	.554E-06	.326E+03	203.21	.000E+00	64.0	.339E+19	.301E+19	.3396+17	,339E+18	.16IE-03	.444E+05	94.99	.910E-03
263.0	1286 11/	1365 + 17	1420-18	12812+16	/0/UE-06	338E+03	202.09	0005+00	62.0	-393E+19	-332E+19	393E+1/	.590E+18	3138-03	.4892 +03	86.23	1458.02
2550	1968.117	1308-17	1560.115	1550 + 16	DISE-06	.394ET03	202.13	0000000	58.0	4336T12 423E±10	4658-110	5238L417	4335-18	2498-03	-04E+05	83.48	1778-02
250.0	1728+17	1538+17	1738+15	1728+16	8208-06	4778+03	200.88	0008+00	560	597E+19	SNR+19	597E+17	997E+18	285E-03	670E+05	81.55	206-02
245.0	.190E+17	169E+17	.191E+15	.190E+16	.907E-06	.\$26E+03	200.20	.000E+00	54.0	677E+19	603E+19	677E+17	.677E+18	.323E-03	749E+05	80.31	.245E-02
240.0	_211E+17	.187E+17	.20E+15	.210E+16	.000E-05	.580E+03	199.48	.000E+00	52.0	.767E+19	.683E+19	,767E+17	.767E+18	.366E-03	.838E+05	79.40	.284E-02
								100-010002-240 0									
235.0	.233E+17	_208E+17	.234E+15	.233E+16	.IIIE-05	.640E+03	198.73	.000E+00	50.0	.869E+19	.773E+19	.869E+17	.869E+18	.414E-03	.940E+05	78.64	.327E-02
230.0	.259E+17	.230E+17	.259E+15	.258E+16	.123E-05	.706E+03	197.95	.000E+00	48.0	.983E+19	.875E+19	.983E+17	.983E+18	.469E-03	.105E+06	78.02	.375E-02
225.0	.287E+17	255E+17	_288E+15	_286E+16	.137E-05	.781E+03	197.13	.000E+00	46.0	.1IIE+20	.991E+19	.111E+18	.IIIE+19	.53IE-03	II9E+06	77.45	.43IE-02
220.0	.319E+17	.284E+17	.320E+15	_318E+16	.152E-05	.863E+03	195.27	.000E+00	44.0	.126E+20	112E+20	.126E+18	.126E+19	60IE-03	.B3E+05	76.96	.494E-02
215.0	.354E+17	.316E+17	.355E+15	.354E+16	.169E-05	.956E+03	195.39	.000E+00	42.0	.143E+20	.127E+20	.143E+18	.143E+19	.683E-03	.150E+06	76.36	_570E-02
230.0	.395E+17		.396E+15	.394E+16	.188E-05	.106E+04	194.47	1000E+00	40.0	.162E+20	.145E+20	.162E+18	.162E+19	.7 ME-03	.169E+05	15.97	603E-02
205.0	.490E+17	_391E+17	.441E+15	.439E+10	.210E-05	.II/E+04	193.52	1000E+00	36.0	183E+20	.163E+20	185E+18	-163E+19	.8/IE-03	191E+00	76.20	/32E-02
198.0	5128-17	4568-117	\$136+15	SI2E+16	244E-05	1365.404	102.55	000E+00	14.0	2315+30	2068+20	231E+19	2312+10	10E-03	241E+06	7612	9185.02
196.0	.535E+17	.477E+17	.537E+15	.535E+16	255E-05	.142E+04	191.75	.000E+00	32.0	.260E+20	.23(E+20	.260E+18	.260E+19	124E-02	.273E+06	77.12	.102E-01
			100710110	100000100	18000 02	in the cost	and the second		1000								
194.0	.560E+17	.498E+17	.56IE+15	.559E+16	.267E-05	.148E+04	191.34	.000E+00	30.0	.29IE+20	.259E+20	.29IE+18	.291E+19	139E-02	.308E+06	77.67	.H3E-01
192.0	.585E+17	.521E+17	.586E+15	.584E+16	.279E-05	.154E+04	190.93	.000E+00	28.0	.325E+20	.289E+20	.325E+18	.325E+19	.155E-02	.347E+06	78.26	.125E-01
190.0	.612E+17	.545E+17	.6I3E+15	.611E+16	.292E-05	.161E+04	190.52	.000E+00	26.0	.363E+20	.323E+20	.363E+18	.363E+19	.173E-02	.390E+06	79.05	.138E-01
188.0	_640E+17	.570E+17	.641E+15	.639E+16	.305E-05	.168E+04	190.10	.100E-04	24.0	.404E+20	.359E+20	.404E+18	_404E+19	.192E-02	.439E+06	79.94	.151E-01
186.0	.670E+17	.5968+17	.671E+15	.669E+16	.3I9E-05	.175E+04	189.67	.100E-04	22.0	.448E+20	.398E+20	.448E+18	.448E+19	.213E-02	.493E+06	81.05	.164E-01
184.0	.700E+17	.024E+17	.702E+15	.700E+16	.334E-05	.183E+04	189.25	.100E-04	20.0	.498E+20	.443E+20	.498E+18	.498E+19	.237E-02	.353E+06	81.87	179E-01
182.0	.755E+17	.05.5E+17	.734E+15	.732E+16	_349E-05	.191E+04	188.82	100E-04	18.0	.551E+20	.4908+20	.551E+18	.3318+19	.263E-02	6038 - 06	83.07	3098-01
120.0	903E 117	215E-117	-709E+15	./00E+10	300E-05	105E-104	168.39	100E-04	10.0	660E+20	.541E+20	560E + 15	.008E+19	3002-02	1093E+00 136E + 06	P4.39	2066-01
1780	B418-17	3498.+17	8428-15	8d0E+16	401E-05	2088-404	187.55	1008-04	14.0	736E - 30	655E-30	736E+18	7368.4-19	3408.00	86482-06	8714	240E-01
.,	2012/17	-CHARTIN	UTLETU	.0-01-110			101-30	1000-04	1230	10003720	2000-20	APOLITIO	1000127	100112-02	0010100	di da	10.0000
174.0	.881E+17	.784E+17	.882E+15	.880E+16	420E-05	227E+04	187.07	.100E-04	10.0	.808E+20	.719E+20	808E+18	.808E+10	.385E-02	.963E406	8863	.256E-01
172.0	.922E+17	.821E+17	.924E+15	.921E+16	.440E-05	238E+04	186.62	100E-04	8.0	.882E+20	.785E+20	.882E+18	.882E+19	.421E-02	.107E+07	90.39	.27IE-01
170.0	.966E+17	.860E+17	.968E+15	.965E+16	.46IE-05	.248E+04	186,17	.100E-04	6.0	.962E+20	856E+20	.962E+18	.962E+19	.459E-02	.119E+07	92.19	.286E-01
168.0	.101E+18	.901E+17	_101E+16	.IO(E+17	.483E-05	.260E+04	185.72	.100E-04	5.0	.100E+2I	893E+20	.100E+19	.100E+20	.478E-02	.125E+07	93.15	.294E-01
166.0	.106E+18	.945E+17	.106E+16	.106E+17	_506E-05	.271E+04	185.27	.100E-04	4.0	.105E+21	.933E+20	.105E+19	.105E+20	.500E-02	.132E+07	93.97	.302E-01
164.0	.111E+18	.990E+17	.IIIE+16	.10E+17	_530E-05	_284E+04	184,81	.100E-04	30	.109E+2I	.970E+20	.109E+19	.109E+20	.520E-02	.139E+07	95.07	.309E-01
162.0	.117E+18	.104E+18	_117E+16	.II7E+17	_556E-05	.297E+04	184.34	.100E-04	2.0	.II3E+21	,101E+21	.II3E+19	II3E+20	.539E-02	.146E+07	96.38	.313E-01
160.0	.122E+18	.109E+18	.122E+16	.122E+17	_583E-05	.30E+04	183.88	.100E-04	1.5	.115E+21	.103E+21	115E+19	.IISE+20	.549E-02	.150E+07	97.08	.315E-01
158.0	.128E+18	.114E+18	.E28E+16	.128E+17	612E-05	.325E+04	183.42	.100E-04	1.0	.117E+21	104E+21	.II7E+19	.II/E+20	.559E-02	153E+07	97.78	.316E-01
136.0	1008+18	-FTOF+18	.U3E+16	.134E+17	.042E-05	.340E+04	182.95	1008-04	.5	198421	JU0E+21	1136+18	.II9E+20	309E-02	.D76+07	98.49	-38E-01
154.0	1418-119	126E+18	MIRAN	MIE / 17	6738-04	356E-104	197 49	1005.04	0	12184.31	1088+31	1216-110	1218 - 30	\$705.03	161E+47	99.20	3208-04
152.0	.148E+18	132E+18	.148E+16	148E+17	207E-05	.372E+04	182.01	100E-04		contra field	credits field	(10 HD 7117	SHEAD TAV	1712 VE	1010-107	20.40	
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# **References** Lellouch, E. & Hunten, D. M. (1987). Titan atmosphere engineering model. ESA Space Science Department Internal Publication, ESLAB 87-199.

- Lellouch, E., Coustenis, A., Gautier, D., Raulin, F, Dubouloz, N. & Frere, C. (1989). Titan's atmosphere and hypothesized ocean: A reanalysis of the Voyager 1 radio occultation and IRIS 7.7 ~m data. *Icarus* 79, 328-349.
- Lindal, G.E., Wood, G.E., Hotz, H. B., Sweetman, D. N., Eshleman, V. R. &Tyler, G. L. (1983). The atmosphere of Titan: An analysis of the Voyager 1 radio occultation measurements. *Icarus* 53, 348-363.
- Smith, G. R., Broadfoot, A. L., Sandel, B. R., Shemansky, D. E., Holberg, J. B. & Strobel, D. E (1982). Titan's upper atmosphere: composition and temperature from the EUV solar occultation results. J. *Geophys. Res.* 87, 1351-1359.
- Steiner, G. & Bauer, S. J. (1990). Molecular and eddy diffusion in the atmosphere of Titan. Ann. Geophys. 8, 473-476.
- Strobel, D. F., Summers, M. E. & Zhu, X. (1992). Titan's upper atmosphere: Structure and ultraviolet emissions. *Icarus* 100, 512-526.
- Strobel, D. F, Hall, D. T., Zhu, X. & Summers, M. E. (1993). Upper limit on Titan's atmospheric argon abundance. *Icarus* 103, 333-336.
- Yelle, R. V. (1991). Non-LTE models of Titan's upper atmosphere. *Astrophys. J.* **383**, 380-400.